九州大学学術情報リポジトリ Kyushu University Institutional Repository

A new tuning approach of Single Input Fuzzy Logic Controller (SIFLC) for Remotely Operated Vehicle (ROV) Depth Control

Fauzal Naim Zohedi

Center for Robotics and Industrial Automation (CeRIA), Fakulti Kejuruteraan Elektrik, Universiti Teknikal Malaysia Melaka

Mohd Shahrieel Mohd Aras

Center for Robotics and Industrial Automation (CeRIA), Fakulti Kejuruteraan Elektrik, Universiti Teknikal Malaysia Melaka

Hyreil Anuar Kasdirin

Center for Robotics and Industrial Automation (CeRIA), Fakulti Kejuruteraan Elektrik, Universiti Teknikal Malaysia Melaka

Mohd Bazli Bahar

Center for Robotics and Industrial Automation (CeRIA), Fakulti Kejuruteraan Elektrik, Universiti Teknikal Malaysia Melaka

https://doi.org/10.5109/4491657

出版情報: Evergreen. 8 (3), pp. 651-657, 2021-09. 九州大学グリーンテクノロジー研究教育センター

バージョン:

権利関係: Creative Commons Attribution-NonCommercial 4.0 International



A new tuning approach of Single Input Fuzzy Logic Controller (SIFLC) for Remotely Operated Vehicle (ROV) Depth Control

Fauzal Naim Zohedi^{1*}, Mohd Shahrieel Mohd Aras¹, Hyreil Anuar Kasdirin¹, Mohd Bazli Bahar¹

¹Center for Robotics and Industrial Automation (CeRIA), Fakulti Kejuruteraan Elektrik, Universiti Teknikal Malaysia Melaka, Malaysia.

> *Author to whom correspondence should be addressed: E-mail: fauzal@utem.edu.my

(Received January 7, 2021; Revised September 6, 2021; accepted September 6, 2021).

Abstract: Remotely Operated Vehicle (ROV) is an important vehicle to do underwater task. The uncertainty environment of underwater make it harder for ROV to maneuver and hold position at certain depth. Research on ROV controller for holding position had been conducted. Proportional, Integral and Derivative (PID), Fuzzy Logic Controller (FLC) and Single Input Fuzzy Logic Controller (SIFLC) was designed and compared. This paper discusses the modelling of developed ROV and tuning the SIFLC to get the best transient response. Steady state error (SSE), percent overshoot (%OS), time rise (Tr) and settling time (Ts) were analyzed to select the best controller. The result shows ROV depth can be controlled more precisely using SIFLC with 1.5 %OS, 11.5s Ts and 7.06s Tr.

Keywords: Remotely operated vehicle; depth control; PID controller; FLC controller and SIFLC controller

1. Introduction

Remotely Operated Vehicle (ROV) is an underwater robot that used to replace human in doing underwater task. It plays very important roles in underwater industries and marine activities. The ROV task can be underwater exploration, oil and gas pipeline monitoring, ship hull cleaning and many more¹⁾. This complicated task need a skilled ROV operator that have the ability to handle two (2) task simultaneously, maneuvering and manipulation of manipulator^{2,3)}. A holding position of ROV need to be achieved to ensure the ROV operator can do manipulation task or underwater observation accurately. Automatic control for holding position is essential to accomplish this³⁾.

Model of the ROV plant need to be developed to implement automatic control. The model is very complex as it has 6 degrees of freedoms. Adding with uncertainty of the underwater environment (hydrodynamics), an accurate model of ROV is very difficult to develop⁴). In this paper, the model of ROV was generated using System Identification (SI) method. The SI method is based on experimental result that generate the relationship of input and output. Figure 1 shows the ROV that was used to in this research project ⁵).



Figure 1: ROV used in the research project

Since the invention of ROV, the depth controller had been designed and developed to hold position of the ROV at certain depth. The most common problem in depth control is high overshoot that can harm ROV or its inspected environment. Several basic controllers had been implemented to ROV depth control⁶⁾⁷⁾. There were PID, FLC, Artificial Neural Network (ANN) and Sliding Mode Control (SMC).

S.M. Zanoli et al ⁸⁾ implemented PID controller to control ROV depth. It can control the ROV but still produce high overshoot. The designed PID was then couple with Continuous Input Smoother (CIS) to cater the problem. It was able to eliminate overshoot but produce slow time response. Z. Tang et al ^{9,10)} state that the simple PID may produce good result but has to tolerate between respond speed and overshoot. S.M. Zanoli et al and Z.

Tang, et al also implement FLC to tuned PID to eliminate overshoot. Result shows a bit oscillation produces before the system stable. A. Nag et al 11) implement FLC to control depth for Autonomous Underwater Vehicle (AUV). The FLC shows adaptability in input changing and very good at tracking. R. Hernández-Alvarado et al 12) use ANN as controller to auto tune PID value to adapt with input changing of ROV depth system. ANN can learn, adapt, and evolve similar as human brain. 13,14) Mean square error (MSE) of conventional PID shows higher value compare to neural network auto tuning PID result. SMC was implemented to ROV depth control by B. Sun, et all¹⁵⁾. A conventional SMC will keep the system as closely as possible to the sliding surface. It will play with switching surface with bang-bang manner. This manner may produce jitter or chattering effect¹⁶). Table 1 shows the advantages and disadvantages of basic controller implemented.

Table 1: Advantages and disadvantages of basic controller

Type of controller	Advantages	Disadvantages
PID	Easy to execute and maintain	only for linear system
FLC	No mathematical modelling required and precise order	complicated in the tuning process
Neural network control	Convergence to a precise model	slower response
Sliding mode control	Non-linear system	Energy wastes occur

From the Table 1, there are advantages and disadvantages of all basic controllers. In this research project, Single Input Fuzzy Logic Controller (SIFLC) which based on FLC was selected. It was a simplified version of FLC where the tuning process was easier compared to tuning FLC itself. It also has normal FLC ability which is model free to cope with ROV uncertainty.

This paper is organized as follows. In Section 1, Introduction of the project is presented, and literature review of the project is discussed. Then, Section 2 establishes the model of ROV using System Identification (SI). Section 3 describes the methodology of the project where controllers designed are discussed. Section 4 illustrate the simulation and analysis of the results. Finally, the final remarks are elucidated in Section 5.

2. System Modelling of ROV

Modelling of ROV plant was generated using SI approach. This approach was based on experimental input output result. ¹⁷⁾¹⁸⁾ From the experimental input output data, a relationship between input output was generated in transfer function. Five (5) steps need to be followed to

implement SI approach ¹⁹⁾. Figure 2 shows the flow chart of SI approach.

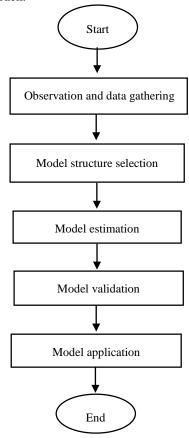


Figure 2: Flow chart of SI approach.

Start with system observation and data gathering, ROV system is observed and the data is gathered. Two sets of input output data were gathered. One (1) set for training and another for validation. The input given to ROV system can be pulse, steps, Random Binary Sequence (RBS), Pseudo Random Binary (PRBS), m-level Pseudo Random (m-PRS) and multi-sine ¹⁹. In this project, multi-sine input was chosen. Then model structure was selected. As MATLAB was used in this project, the Instrument Variable (IV) approach was selected. Next, the selected model structure is implemented for model estimation and model validation to generate a ROV model. Lastly, the model generated is used to design ROV controller.

For this developed ROV, pressure sensor was used to measure depth of the ROV. This was based on the pressure depth equation as shown in Equation (1).

$$P = \rho g h \tag{1}$$

Pressure due to weight of liquid is given by Eq. (1), where P is pressure, ρ (103kg/m3 or g/mL) is the density of the liquid (water = 1 and sea water = 1.025) , g is the acceleration due to gravity (g=9.80m/s2) and h is the height of the liquid.

The deeper the ROV gone, the more pressure will be

produced. From this relation, and input output experimental data was gathered where the offset is set to 1.5m. Three (3) sinusoid inputs with difference frequencies; 0.5, 2 and 5 rad/s were given to the ROV system ¹⁹⁾. To gain an ideal result, the experiment was conducted in a controlled environment. Disturbance was not considered. The data was shown as Figure 3.

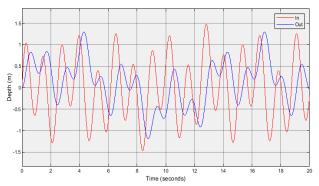


Figure 3: Input output data to do system identification (SI)

The input data was the depth set point while the output data is the the actual depth. From the data shown Figure 2, transfer function of the system was generated using MATLAB System Identification (SI) method was shown in Eq. (2). The setup selected was instrument variable approach; IV and 3 poles and 2 zeros transfer function. The best fitting match shown 96.43%. It was acceptable because within 80% to 99% best fits.

$$H(S) = \frac{0.02332s^2 + 0.04058s + 0.01126}{s^3 + 0.7114s^2 + 0.1861s + 0.01398}$$
(2)

The generated output transient response was shown in Figure 4.

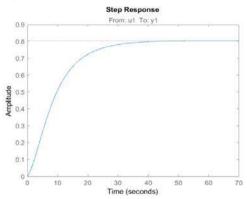


Figure 4: Transient response of the ROV model

The generated transient response was then analyzed in term of percent overshoot (%OS), steady state error (SSE), rise time (Tr) and settling time (Ts). The data was tabulated in Table 2.

Table 2: Original ROV heave transient response

	%OS $Tr(s)$ $Ts(s)$			
Original	0	17.178	40.16	0.22

3. Controller Design

Three approaches for Controller design were PID controller, Fuzzy Logic controller (FLC) and Single-Input FLC (SIFLC). To implement the controllers, the developed ROV system was studied. The developed ROV uses 12V DC motor thruster to maneuver from one place to another. It was an under actuated ROV as it contained only 4 thrusters. 2 thrusters for forward or reverse (surge) and turn right or left (yaw). Another 2 thrusters use for dive and emerge (heave). The depth set point given to the ROV system and maneuver the ROV to the specific depth. Feedback given by pressure sensor sense in voltage was converted to depth and compared with input setpoint. Figure 5 shows a closed loop transient response for the plan. Table 3 shows the closed loop ROV performances in terms of OS%, Tr, Ts and SSE.

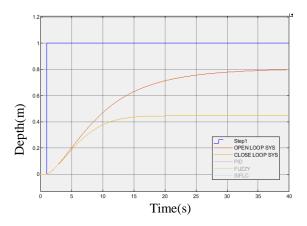


Figure 5: Open Loop and closed loop transient response

Table 3: Close loop ROV heave transient response

	%OS	Tr(s)	Ts(s)	SSE
Close loop	0	8.913	16.7	0.54

Even the close loop response has better Ts and Tr compared to open loop, it has higher SSE compare the open loop system as shown in Table 2 and Table 3. It does not even reach half of the set point given. Based on the errors in the open loop and close loop result, PID, FLC and SIFLC was designed.

3.1. PID controller

Conventional PID controller is the most common or basic controller used to ROV system. The P, I, and D blocks were put in parallel in front of the plan to control the system. The P counter the direct error; the I indicate the total errors in the system while D shows how fast to the errors happen. The P controller will make the response faster but intend to produce overshoot. The I controller tend to eliminate SSE while the D controller decrease overshoot. The summarize effect of PID is shown in Table 4.

DD 11 4	TICC .	c ·			CDID
	Hittect	of inc	reacing	parameters	0 t PII 1

Parameter	Tr	%OS	Ts	SSE
Кр	Decrease	Increase	A bit	Decrease
			change	
Ki	Decrease	Increase	Increase	Eliminate
Kd	A bit	Decrease	Decrease	No effect
	change			

The PID controller block diagram is shown as in Figure 6. The P, I and D are connected in parallel between each other and placed in series within the depth block diagram. The PID was tuned using automatic tuning in MATLAB Simulink²⁰).

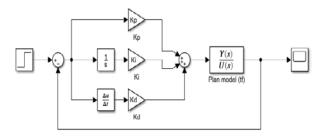


Figure 6: PID controller block diagram.

3.2. Fuzzy Logic Controller (FLC)

FLC was introduced by Lotfi A Zadeh in 1965 ²¹⁾. This controller was based on human decision making and can implement linguistic decision. ²²⁾ There are 4 basic components in FLC shown in Figure 7. ²³⁾²⁴⁾

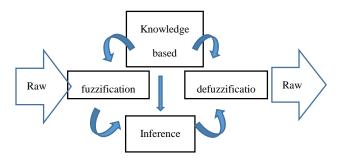


Figure 7: Basic configuration of FLC components.

Two (2) inputs were selected which are errors and differential errors or errors rate. The rules for decision making of FLC can be varies from 3 X 3 to 7 X 7 or even more. The less numbers of rules may lessen the computational time and faster the output result. In this project 7 X 7 fuzzy rules were selected. Table 5 shows the rules table for depth control of ROV.

Table 5: Rules table for depth control of ROV

err vs du/dt	PL	PM	PS	Z	NS	NM	NL
NL	Z	NS	NM	NL	NL	NL	NL
NM	PS	Z	NS	NM	NL	NL	NL
NS	PM	PS	Ž	NS	NM	NL	NL
Z	PL	PM	PS	Ž	NS	NM	NL
PS	PL	PL	PM	PS	Ž	NS	NM
PM	PL	PL	PL	PM	PS	Z	NS
PL	PL	PL	PL	PL	PM	PS	Z
						_	a

3.3. Single Input FLC (SIFLC)

SIFLC is an improvisation of FLC to make it simplified and easier to tuned. It has only one (1) input compare to two (2) input that FLC used. Theoretically SIFLC output result should be identical to FLC. Figure 8 shows the basic block diagram of SIFLC ²⁵⁾²⁶⁾.

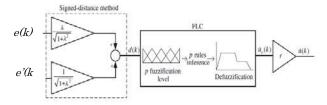


Figure 8: Basic SIFLC block diagram.

Two (2) input of FLC; error and differential of error were converted to d using signed distance method (SDM). 'd' is the distance between two (2) points; Q and P as shown in Figure 9. Line 'a' and 'b' are the line created based on pattern in the Table 5. 'a' is the main diagonal line while 'b' is the first 1st diagonal line to the right. Eq. (3) is the equation of the main diagonal line.

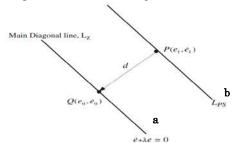


Figure 9: Derivation of d, distance between point Q and P²⁵⁾

$$e' + (e)\lambda = 0 \tag{3}$$

$$d = \left(e(k) \times \frac{\lambda}{\sqrt{1+\lambda^2}}\right) + \left(e'(k) \times \frac{\lambda}{\sqrt{1+\lambda^2}}\right) \tag{4}$$

3.4 Tuning FLC and SIFLC

SIFLC was designed based on FLC designed. As discussed in the previous subchapter, the relation of 2 diagonal line was used to reduce the input of FLC to single input (Eq. (4)). In this research project, the gradient (λ) of line was varying heuristically up and down to tune the

output transient result of SIFLC. The (λ) linked to the FLC by the input of the FLC. The range of error and integral error was plotted in a graph shown in Figure 10.

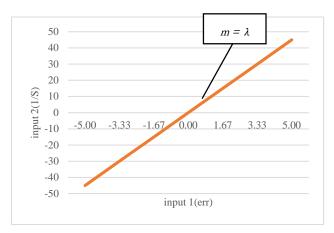


Figure 10: Plotted graph of input 2 versus input 1 FLC.

The varying of (λ) SIFLC result was then analyzed, and the best result was selected. Then the best gradient was used to redesign the input range of FLC to get better result of FLC.

Figure 11 shows the simulation block diagram for this research project. Six (6) signals were compared to analyze the best controller for the ROV. The signals were step input, open loop, closed loop, PID, FLC and SIFLC.

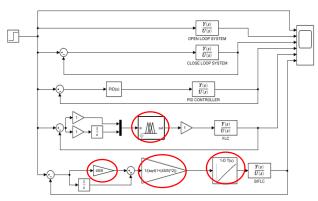


Figure 11: Block diagram for step input, open loop, closed loop, PID, FLC and SIFLC.

The highlighted block in Figure 11 was the block that affected by the retuned of (λ) value. The retuning of (λ) value affected the 'd' value as Eq. (4). Due to that, the truth table of 'd' versus output was also affected. Lookup table in the block diagram need to be change based on the retuned 'd' value. For the FLC, once SIFLC tuning was done, the range of error and integral error was adjusted as the (λ) was basically the gradient of input 1 and input 2 in FLC. Figure 12 shows the flow diagram of the tuning process.

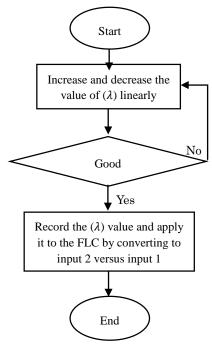


Figure 12: Flow diagram for SIFLC and FLC tuning

In Figure 10 mentioned previously, the (λ) value or the gradient was already at the best condition of the ROV system. Before tuned, the value of (λ) was 5 where input 2 versus input 1 was 10/2. After tuned, the value of (λ) was 9 where the value of input 2 versus input 1 was 45/5. The 'd' truth table for lookup table was change as shown in from Table 6 to Table 7.

	Table 6: 'd' truth table before tuned									
In 1	-2.0	-1.33	-0.67	0.0	0.67	1.33	2.0			
In 2	-10	-6.67	-3.33	0	3.33	6.67	10			

Table 7: 'd' truth table after tuned								
In 1	-5.0	-3.33	-1.67	0.0	1.67	3.33	5.0	
In 2	-45	-30	-15	0	15	30	45	

4. Results and Discussion

Figure 13 shows the result of all 6 signals implemented to the system before the tuning of SIFLC implemented.

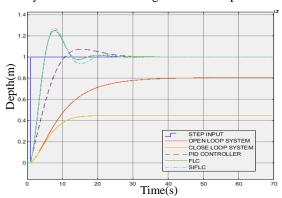


Figure 13: 6 signals implemented to the system before the tuning of SIFLC implemented

Directly from Figure 13 can be seen that the FLC and SIFLC have the highest %OS. It was led by SIFLC. Close loop and open loop show the highest SSE produced. PID shows the most relevant controller shown but slower in term of Tr. Then, the SIFLC was retuned by using heuristic method where the gradient (λ) was varies. Next based on SIFLC result, FLC was retuned. The result was shown as below in Figure 14.

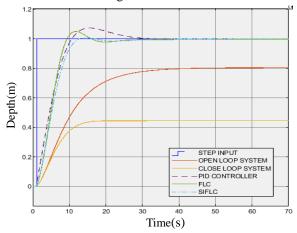


Figure 14: Retuned of SIFLC and FLC result

Table 6: Performance of PID and SIFLC controller

Controller	%OS	Tr(s)	Ts(s)	SSE
PID	6.989	7.07	27.1	0.0017
FLC	24.375	3.03	15.7	0.0011
SIFLC	27.564	2.983	18.15	0.0109
FLC (new)	5.851	5.245	18.9	0.0131
SIFLC (new)	1.531	7.057	11.52	0.0027

The performance of all controllers was tabulated in Table 6. The new tuned SIFLC and FLC shows tremendous recovery in the %OS but compensated by Tr value. In terms of Ts value, SIFLC lead all other controllers. For SSE, all controllers produced acceptable result and compensate either the original system or close loop system.

From result, all controllers simulated can be used for ROV control, however %OS value produced may damage the ROV or its investigated environment. From all presented result, retuned SIFLC is the best as it has the best %OS. PID controller is stronger in linear systems, but FLC is suitable for linear and non-linear system. SIFLC is adapting the FLC ability but with single input. SIFLC also shows better stability and overshoot. In terms of tuning aspect, PID is easier compared to FLC but SIFLC seams to simplify complexity of tuning the FLC because of the single input.

5. Conclusion

Three controllers had been successfully implemented to ROV depth system. SIFLC shows the best performance as it eliminates %OS and have the best Ts value. It adapts FLC ability which are model free and adaptable to cater disturbance and non-linearity system. The single input simplifies the FLC tuning process. Tuning the λ value is proven can improve the transient response of SIFLC and can be used to retuned FLC. Compared to PID, it was easy to tune but highly depends on linear model. For future research, it the controller will be tested experimentally, and optimization will be embedded in the system to cater the varies effect of set point.

Acknowledgement

We wish to express our gratitude and appreciation the support granted by Universiti Teknikal Malaysia Melaka in pursuing this research specially to Underwater Technology Research Group, Faculty of Electrical Engineering, Centre of Research, and Innovation Management for supporting this research.

References

- E.H. Binugroho, Wafiqqurochman, M.I. Mas'Udi, B. Setyawan, R.S. Dewanto, and D. Pramadihanto, "EROV: depth and balance control for rov motion using fuzzy pid method," IES 2019 Int. Electron. Symp. Role Techno-Intelligence Creat. an Open Energy Syst. Towar. Energy Democr. Proc., 637–643 (2019). doi:10.1109/ELECSYM.2019.8901673.
- 2) K.R. Goheen, and E.R. Jefferys, "Multivariable self-tuning autopilots for autonomous and remotely operated underwater vehicles," IEEE J. Ocean. Eng., 15 (3) 144–151 (1990). doi:10.1109/48.107142.
- M.S.M. Aras, and S.S. Abdullah, "Adaptive simplified fuzzy logic controller for depth control of underwater remotely operated vehicle," Indian J. Geo-Marine Sci., 44 (12) 1995–2007 (2015).
- B. Huang, and Q. Yang, "Double-loop sliding mode controller with a novel switching term for the trajectory tracking of work-class rovs," Ocean Eng., 178 (March) 80–94 (2019). doi:10.1016/j.oceaneng.2019.02.043.
- 5) M.S.M. Aras, S.S. Abdullah, M.Z.A. Rashid, A.A. Rahman, and M.A.A. Aziz, "Development and modeling of unmanned underwater remotely operated vehicle using system identification for depth control," J. Theor. Appl. Inf. Technol., 56 (1) 136–145 (2013).
- 6) M.S.M. Aras, S.S. Abdullah, and F.A. Azis, "Review on auto-depth control system for an unmanned underwater remotely operated vehicle (rov) using intelligent controller," J. Telecommun. Electron. Comput. Eng., 7 (1) 47–55 (2015).
- Z. Yuguang, and Y. Fan, "Dynamic modeling and adaptive fuzzy sliding mode control for multi-link underwater manipulators," Ocean Eng., 187 (April) 106202 (2019). doi:10.1016/j.oceaneng.2019.106202.
- 8) S.M. Zanoli, and G. Conte, "Remotely operated vehicle depth control," Control Eng. Pract., 11 (4) 453–459 (2003). doi:10.1016/S0967-

- 0661(02)00013-8.
- 9) Z. Tang, Luojun, and Q. He, "A fuzzy-pid depth control method with overshoot suppression for underwater vehicle," Lect. Notes Comput. Sci. (Including Subser. Lect. Notes Artif. Intell. Lect. Notes Bioinformatics), 6329 LNCS (PART 2) 218–224 (2010). doi:10.1007/978-3-642-15597-0_24.
- 10) Z. Tang, P. Yan, and Luojun, "A novel rov depth control based on lsm fitting predictor and fuzzy compensation," ICACTE 2010 2010 3rd Int. Conf. Adv. Comput. Theory Eng. Proc., 2 V2-612-V2-614 (2010). doi:10.1109/ICACTE.2010.5579496.
- 11) A. Nag, S.S. Patel, and S.A. Akbar, "Fuzzy logic based depth control of an autonomous underwater vehicle," Proc. 2013 IEEE Int. Multi Conf. Autom. Comput. Control. Commun. Compress. Sensing, IMac4s 2013, 117–123 (2013). doi:10.1109/iMac4s.2013.6526393.
- 12) R. Hernández-Alvarado, L.G. García-Valdovinos, T. Salgado-Jiménez, A. Gómez-Espinosa, and F. Fonseca-Navarro, "Neural network-based self-tuning pid control for underwater vehicles," Sensors (Switzerland), 16 (9) 1–18 (2016). doi:10.3390/s16091429.
- 13) N. Weake, M. Pant, A. Sheoran, A. Haleem, and H. Kumar, "Optimising parameters of fused filament fabrication process to achieve optimum tensile strength using artificial neural network," Evergreen, 7 (3) 373–381 (2020).
- 14) H. Han, M. Hatta, and H. Rahman, "Smart ventilation for energy conservation in buildings," Evergreen, 6 (1) 44–51 (2019). doi:10.5109/2321005.
- 15) B. Sun, and D. Zhu, "A chattering-free sliding-mode control design and simulation of remotely operated vehicles," Proc. 2011 Chinese Control Decis. Conf. CCDC 2011, 4173–4178 (2011). doi:10.1109/CCDC.2011.5968958.
- 16) L.G. García-Valdovinos, F. Fonseca-Navarro, J. Aizpuru-Zinkunegi, T. Salgado-Jiménez, A. Gómez-Espinosa, and J.A. Cruz-Ledesma, "Neuro-sliding control for underwater rov's subject to unknown disturbances," Sensors (Switzerland), 19 (13) (2019). doi:10.3390/s19132943.
- 17) T.N. Dief, and S. Yoshida, "System identification for quad-rotor parameters using neural network," Evergreen, 3 (1) 6–11 (2016). doi:10.5109/1657380.
- 18) T.N. Dief, and S. Yoshida, "System identification and adaptive control of mass-varying quad-rotor," Evergreen, 4 (1) 58–66 (2017). doi:10.5109/1808454.
- 19) M.H.F. Taib, M. N., Adnan, R. and Rahiman, "Practical System Identification," in: Penerbit UiTM, 2007: p. 600.
- 20) J. Ko, N. Takata, K. Thu, and T. Miyazaki, "Dynamic modeling and validation of a carbon dioxide heat pump system," Evergreen, 7 (2) 172–194 (2020). doi:10.5109/4055215.
- 21) L.. Zadeh, "Zadeh_FuzzySetTheory_1965.pdf," Inf.

- Control, 8 338-353 (1965).
- 22) M.A. Berawi, S.A.O. Siahaan, Gunawan, P. Miraj, and P. Leviakangas, "Determining the prioritized victim of earthquake disaster using fuzzy logic and decision tree approach," Evergreen, 7 (2) 246–252 (2020). doi:10.5109/4055227.
- 23) M.S.M. Aras, S.N.B.S. Salim, E.C.S. Hoo, I.A.B.W.A. Razak, and M.H. Bin Hairi, "Comparison of fuzzy control rules using matlab toolbox and simulink for dc induction motor-speed control," SoCPaR 2009 -Soft Comput. Pattern Recognit., 711–715 (2009). doi:10.1109/SoCPaR.2009.143.
- 24) M.S. Bin Mohd Aras, S.M.S.B. Syed Abdul Hamid, F.B.A. Azis, F.A.B. Ali, and S. Shah B Abdullah, "Study of the effect in the output membership function when tuning a fuzzy logic controller," Proc. 2011 IEEE Int. Conf. Control Syst. Comput. Eng. ICCSCE 2011, 1–6 (2011). doi:10.1109/ICCSCE.2011.6190485.
- 25) K. Ishaque, S.S. Abdullah, S.M. Ayob, and Z. Salam, "Single input fuzzy logic controller for unmanned underwater vehicle," J. Intell. Robot. Syst. Theory Appl., 59 (1) 87–100 (2010). doi:10.1007/s10846-010-9395-x.
- 26) M.S.M. Aras, A.M. Kassim, A. Khamis, S.S. Abdullah, and M.A.A. Aziz, "Tuning factor the single input fuzzy logic controller to improve the performances of depth control for underwater remotely operated vehicle," Proc. UKSim-AMSS 7th Eur. Model. Symp. Comput. Model. Simulation, EMS 2013, 3–7 (2013). doi:10.1109/EMS.2013.1.