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Temperature dependent thermal conductivity of a suspended submicron graphene ribbon

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Thermophysical characterization of graphene is very important for both fundamental and technological research. While most of the existing thermal conductivity measurements are for graphene sheets with sizes larger than 1 μ m, the thermal conductivities for suspended submicron graphene ribbons are still very few, although the thermal conductivity of graphene ribbons at the submicron scale is predicted to be much smaller than large graphene and strongly size dependent for both length and width due to the 2D nature of phonon transport. Here, we report the temperature dependent thermal conductivity of a 169-nm wide and 846-nm long graphene ribbon measured by the electrical self-heating method. The measured thermal conductivities range from (12.7 ± 2.95) W/m/K at 80 K to (932 ± 333) W/m/K at 380 K, being (349 ± 63) W/m/K at 300 K, following a $\sim T^{2.79}$ law for the full temperature range of 80 K to 380 K and a $\sim T^{1.23}$ law at low temperatures. The comparison of the measured thermal conductance with the ballistic transport limit indicates diffusive transport in this narrow and short ribbon due to phonon-edge as well as phonon-defect scattering. The data were also combined with an empirical model to predict possible width dependence of thermal conductivity for suspended graphene ribbons. These results help understand the 2D phonon transport in suspended submicron graphene ribbons and provide knowledge for controlling thermophysical properties of suspended graphene nanoribbons through size manipulation. © 2015 AIP Publishing LLC. [http://dx.doi.org/10.1063/1.4907699]

I. INTRODUCTION

As a 2D material with superior thermal conductivity, graphene is regarded as a good candidate for thermal management in nano devices and its thermophysical characterization is very important for both fundamental research and technological applications.¹ The first few measured thermal conductivities of graphene were obtained by Balandin et al.^{2,3} using a Raman spectroscopy technique and the $\sim 10 \,\mu m$ long suspended exfoliated graphene samples were measured to have thermal conductivities of 4000-5300 W/m/K, superior to both diamond and carbon nanotubes. However, the following several Raman based measurements^{4–7} showed much smaller thermal conductivities for micro size suspended graphene samples, ranging from 600 W/m/K to about 2000 W/m/K at room temperature. The large discrepancy of Raman based data mainly resulted from the low sensitivity of Raman signals with respect to temperature as well as the estimation of laser absorption.⁸ In the Raman based measurements, the temperature rise at the laser spot should be $\sim 50 \,\mathrm{K}$ to acquire enough temperature accuracy and thus the measured temperature dependent thermal conductivities also had large error bars in the temperature axis.⁵ For more accurate electricalheating based measurement, Seol *et al.*⁹ fabricated suspended beams of graphene/SiO₂ (1.5–3.2 μ m wide, 9.5–12.5 μ m long) on a Si wafer coated with Au films and obtained the thermal conductivity of supported graphene to be about 600 W/m/K at room temperature, with strong interfacial phonon scattering between graphene and SiO₂. Several groups^{10–13} successfully integrated graphene with prepatterned SiN/Pt membranes and measured the thermal conductivity of both supported and suspended graphene sheets using the thermal bridge method. Besides, Xie *et al.*¹⁴ employed the four-wire electrical selfheating method to measure the thermal conductivity of a large graphene sheet with 385 μ m width and 508 μ m length based on the almost linear relationship of graphene's electrical resistance and temperature at 200 to 380 K.

On the other hand, most of the measured graphene samples were several micrometers in size, while the thermal conductivity data of submicron graphene ribbons are still limited, especially for suspended samples, probably due to the fabrication difficulty of suspending this atom thick layer. The intrinsic mean free path of graphene is about 500 nm for suspended graphene and 100 nm for SiO₂ supported graphene¹⁵ and thus the thermal conductivity is strongly size dependent for submicron graphene ribbons. The phonon transport process will be quasi-ballistic when the length of a

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graphene ribbon is shortened to be comparable with the intrinsic mean free path while the width is large enough.^{11,15} When the width is narrowed down to be comparable with the intrinsic mean free path, the phonon scattering with edge roughness begins to dominate the phonon transport process and the transport process will be diffusive with the free path shortened by the edges.¹⁵ An elastic-shell-based calculation¹⁶ showed that the ballistic thermal conductance per unit cross section, which does not depend on the length, varies with the width for graphene ribbons narrower than 500 nm but becomes independent of width for ribbons wider than 500 nm. Bae et al.¹⁵ measured the thermal conductivities of SiO₂ supported graphene ribbons with 260 nm length and 45 nm, 65 nm, 85 nm, and 130 nm widths using a metal heater and sensor and the thermal conductivity scaled with width approximately as $\sim W^{1.8\pm0.3}$, being about 250 W/m/K for the 130 nm wide ribbon at 300 K. Xu et al.¹¹ measured the length-dependent thermal conductivity of suspended monolayer graphene ribbons with a fixed width of $1.5 \,\mu m$ and lengths ranging from 300 nm to 9 μ m and obtained thermal conductivities logarithmically divergent with the sample lengths even for graphene ribbons much longer than the intrinsic phonon mean free path. Xu and co-workers¹¹ also provided temperature dependent thermal conductivities of a graphene ribbon with $4 \,\mu m$ width and $2.5 \,\mu m$ length and demonstrated that the thermal conductivity was weakly width dependent when the width was larger than $1.5 \,\mu\text{m}$. Xu and co-workers¹¹ also suggested that the suspended ribbons could be more strongly width dependent than supported samples. However, the thermal conductivity data for suspended submicron graphene ribbons are still very few, although the thermal conductivity is predicted to be strongly dependent with both length and width at sub-micrometer scale for suspended ribbons due to the 2D nature of heat flow in graphene.

Here, we report the temperature dependent thermal conductivity of a suspended graphene ribbon with 169 nm width and 846 nm length measured by the four-wire electrical self-heating method^{14,17,18} based on the temperature dependent electrical resistance at 80 K to 380 K. This work will help understand the size dependent phonon transport at sub-micrometer scale.

II. EXPERIMENT

A. Sample fabrication

The four-wire electrical self-heating method was used to measure the thermal conductivity of graphene and the electrical current was passed through the suspended graphene ribbon via Au/Cr electrodes deposited onto the graphene ribbon. The main fabrication processes are shown in Fig. 1. First, a large-area graphene sheet grown by Cu-based chemical vapor deposition (Cu-CVD) was transferred to a $10 \times 10 \text{ mm Si/SiO}_2$ wafer with the help of PMMA. The details of the graphene growth and transfer were described elsewhere.^{19,20} Then, the graphene sheet was patterned into a 500 μ m long, ~200 nm wide ribbon via electron beam lithography followed by O2 plasma etching. In a second e-beam lithography step, 8 nm Cr and 30 nm Au patterns were physical vapor deposited onto the Si wafer as four electrodes, clamping the graphene nanoribbon and ensuring good electrical and thermal contact. Finally, the graphene ribbon was suspended by etching 200 nm thick SiO₂ via buffered hydrofluoric acid (BHF) and dried using a CO2 critical point dryer to avoid damage from surface tension.

Figs. 2(a) and 2(b), respectively, show the top view and tilt 60° view SEM images of the suspended graphene ribbon. The suspended part was 169 nm wide and 846 nm long and the thickness was taken as 0.335 nm.¹⁶ Figs. 3(a) and 3(b), respectively, show the Raman spectra and band intensity ratio of the graphene sample. In Fig. 3(a), Raman spectra (1)–(4), respectively, show the spectra after the large-area graphene was transferred onto the Si/SiO₂ wafer (1), after O₂ plasma patterning (2), right after ribbon suspending by BHF etching and critical point dry (3), and after SEM observation (4). Before O₂ plasma etching, the Raman spectrum showed



FIG. 1. Main fabrication process of the suspended graphene nanoribbon with 4 Au/Cr electrodes.



FIG. 2. SEM images of the suspended graphene ribbon (169×846 nm). (a) Top view; (b) tilt 60° view.

no D band (no defects) and the 2D band intensity was almost twice of G band, indicating high quality of the monolayer graphene.¹⁵ After O₂ plasma patterning, the Raman spectrum of Fig. 3(a) (2) showed notable D band and the intensity ratio of the D band to the G band, I_D/I_G , was 0.3, indicating the effects of edge disorder for this narrow ribbon.¹⁵ Actually, $I_{\rm D}/I_{\rm G}$ varies with the width of graphene ribbons, as shown in Fig. 3(b), where the square symbols are the reference data¹⁵ for 260 nm long ribbons and the sphere symbol is the present data from Fig. 3(a) (2), indicating increasing influence of the edge disorder as the graphene ribbon is narrowed. Right after the graphene ribbon was suspended by BHF etching and critical point dry, the Raman spectrum of Fig. 3(a) (3) showed some noise caused by the residue from the wet etching and drying processes and tilt baseline caused by the laser reflection from the adjacent metal electrodes, while the intensity ratio, $I_{\rm D}/I_{\rm G}$, was 0.5. After SEM observation for confirming the ribbon suspension, the D band was significantly enhanced with $I_{\rm D}/I_{\rm G}$ becoming 1.0, indicating the graphene ribbon was defected by the electron beam. However, the graphene quality after SEM observation was still better than the 130 nm wide ribbon as shown in Fig. 3(b).

B. Measurement method

The suspended graphene nanoribbon was heated by direct current and the average temperature rise can be detected through the electrical resistance based on the temperature-resistance relationship of the graphene nanoribbon. The thermal conductivity of the nanoribbon, λ , can be extracted from the one dimensional heat conduction equation and can be expressed as Eq. (1)^{17,18}

$$\lambda = \frac{R'l}{12wh} \frac{\mathrm{d}P}{\mathrm{d}R},\tag{1}$$

where *l* is the nanoribbon length, *w* is the nanoribbon width, *h* is the nanoribbon thickness (0.34 nm); *R* is the electrical resistance, *P* is the electrical power, dP/dR is the slope of the *P*-*R* curve; R' = dR/dT is the slope of the calibrated *R*-*T* curve at the ambient temperature.

During the measurement, $0.2-25 \,\mu\text{A}$ direct currents (Power supplier: Advantest R6243) were passed through the suspended graphene nanoribbon via Au/Cr electrodes in a vacuum chamber (Oxford Instruments Optistat CF-V-KT). Pressures were lower than 5×10^{-4} Pa and the heat loss from the nanoribbon to the environment could be neglected. The graphene nanoribbon was connected to a $1 \text{ k}\Omega$ standard resistor (Yokogawa 2792 Standard Resistor) and the electrical current was measured from the voltage of the standard resistor. The voltages of the graphene nanoribbon and the standard resistor were measured by 8.5-digit Keithley 2002 Multimeters. As for the thermal contact resistance at the Au/ Cr/graphene/SiO₂ interfaces, several measurements^{7,21,22} showed that the thermal interfacial resistance is on the order of 10^{-8} m²K/W. In our device, the contact part at each electrode is a long ribbon of $\sim 250 \,\mu m$ length and $\sim 200 \,nm$ width. Assuming that the effective contact area is $100 \,\mu\text{m} \times 200 \,\text{nm} = 20 \,\mu\text{m}^2$ and that the thermal interfacial resistance is 10^{-7} m² K/W, the total thermal contact resistance will be 1×10^4 K/W. Taking the thermal conductivity of the suspended graphene ribbon as 1000 W/m/K, the thermal resistance of the suspended ribbon will be 1.5×10^7 K/ W. The thermal contact resistance is 0.07% of the suspended ribbon's thermal resistance and thus can be neglected.

III. RESULTS AND DISCUSSION

Figs. 4 and 5, respectively, show the temperature dependent electrical resistance and electrical conductivity of the suspended graphene nanoribbon at 80 K to 380 K. Low currents of $0.2-2 \,\mu$ A were used to determine the electrical resistance and the error bars in Figs. 4 and 5 indicate the data dispersion at low currents. The electrical conductivity increases from 8.2×10^8 to $9 \times 10^8 \,\Omega^{-1} \,\mathrm{m^{-1}}$, which is on the same order as large graphene sheets, ¹⁴ as the temperature rises from 80 K to 380 K. The electrical resistance does not linearly change with temperature at the full temperature range but can be regarded locally linear at the specific temperature. Especially at 260 K to 360 K, the electrical



FIG. 3. Raman spectra and band intensity ratio of the graphene sample. (a) Raman spectra of the graphene sample during the fabrication processes: (1) after the large-area graphene was transferred onto the Si/SiO₂ wafer; (2) after O₂ plasma patterning; (3) right after suspending by BHF etching and critical point dry; (4) after SEM observation. (b) Intensity ratio of the D band and the G band varying with the width after O₂ plasma patterning, where the square symbols are taken from Ref. 15 for 260 nm long ribbons and the sphere symbol is the present data from Fig. 3(a) (2).

resistance changes almost linearly with temperature and the *R*-*T* slope is $-2.612 \text{ }\Omega/\text{m}$, as shown in the inset of Fig. 4.

The local slope of the *R*-*T* curve, R' (=d*R*/d*T*), can be approximated by linear fitting the adjacent data at the specific temperature, as shown in Fig. 6. Fig. 7 shows the slope of the *P*-*R* curve, d*P*/d*R*, changing with temperature and the inset shows some representative *R*-*P* curves at 80 to 380 K when 3–25 μ A currents were passed through the suspended ribbon and the electrical powers were within 10 μ W. As can be seen from the inset of Fig. 7, the R-P curves were not linear for the full power range but sectionally linear, indicating nonlinear *R*-*T* relationship. For the calculation of d*P*/d*R*,



FIG. 4. Temperature dependent electrical resistance of the suspended graphene nanoribbon. Inset: Linear fitting between 260 K and 360 K.



FIG. 5. Temperature dependent electrical conductivity of the suspended graphene nanoribbon.



FIG. 6. Temperature dependent R' (=dR/dT) of the suspended graphene nanoribbon.



FIG. 7. Temperature dependent dP/dR of the suspended graphene nanoribbon. Inset: representative *R-P* curves at 380 K, 300 K, 210 K, 150 K, 120 K, and 80 K with currents from 3 to ~25 μ A.

only the first 5 to 10 data were used to fit the linear slope, ensuring that the maximum temperature rises were within 10 K and the error bars in Fig. 7 show the dispersion of the linear fitting results.

Combining R', dP/dR and the dimensions of the suspended ribbon, we can calculate the thermal conductivity of the suspended nanoribbon using Eq. (1) and Fig. 8 shows the temperature dependent thermal conductivity with the inset showing the low temperature results. The thermal conductivities can be fit to a $\sim T^{2.79}$ relationship at the full temperature range of 80 to 380 K, while at low temperatures of 80 to 130 K, the thermal conductivities can be fit to $a \sim T^{1.23}$ relationship, being (349 ± 63) W/m/K at 300 K, (932 ± 333) W/m/K at 380 K, and (12.7 ± 2.95) W/m/K at 80 K. The present data are much smaller than the thermal conductivity of large graphene sheets, which is about 2000 W/m/K at room temperature, but consistent with the reference data for a SiO₂-supported ribbon with 130 nm width and 260 nm length $(\sim 250 \text{ W/m/K} \text{ at } 300 \text{ K})^{15}$ and a suspended ribbon with 3 μ m width and 500 nm length (190 W/m/K at 280 K).¹⁰



FIG. 8. Temperature dependent thermal conductivity of the suspended graphene nanoribbon, fit to $a \sim T^{2.79}$ relationship at 80 K to 380 K. Inset: low temperature 80–130 K data can be fitted to $a \sim T^{1.23}$ relationship.

Besides, theoretical work^{16,23} has predicted that the low temperature thermal conductivity of graphene follows $a \sim T^{\alpha}$ law, where α varies from 1 for a nanoribbon of ~ 4 nm width to 1.5 for graphene sheets with width larger than 500 nm. Xu *et al.*¹⁰ also obtained $a \sim T^{1.53}$ law for a suspended 3- μ m wide ribbon at temperatures below 150 K. Our present $\sim T^{1.23}$ law for this 169-nm wide ribbon at low temperatures is in accordance with the theoretical prediction for graphene ribbons narrower than 500 nm.

If the graphene sample is wide and short, which means the length is submicron while the width is larger than 1 μ m, the phonon transport process will be quasi-ballistic and the thermal conductance per unit cross section, *G*/A, will be more instructive than the thermal conductivity.^{10,11,15,16,21} Theoretical work¹⁵ showed that the simulated ballistic thermal conductance per unit cross section of clean graphene, *G*_{ball}/A, can be fitted as

$$G_{\text{ball}}/A = [1/(4.4 \times 10^5 T^{1.68}) + 1/(1.2 \times 10^{10})]^{-1} \,\text{WK}^{-1}\text{m}^{-2},$$
(2)

when the temperature ranges from 1 K to 1000 K. Fig. 9 shows the thermal conductance per unit cross section, G/A, of the present short and narrow suspended ribbon and the magenta line indicates the ballistic limit. The measured thermal conductance is 2.3% of the predicted ballistic limit at 80 K and 21% at 380 K. While the reference thermal conductance for wide and short graphene samples was 30%-40% of the ballistic limit, 10,11,15 our measured data show deviation from quasi-ballistic transport, indicating the fact that the transport in this narrow and short ribbon is indeed diffusive due to phonon-edge scattering. Besides, the sample quality was reduced to some degree during the SEM observation process, as shown in the Raman spectra, which also contributed to phonon-defect scattering and caused deviation from ballistic transport.

The present data can also be extrapolated to predict possible width dependence of thermal conductivity for suspended nanoribbons using a simple empirical model^{11,15} expressed by Eq. (3)



FIG. 9. Temperature dependent thermal conductance per unit cross section, G/A. The magenta line indicates the ballistic limit of wide graphene sheets.¹⁵

where $\lambda_{\text{eff}}(W, L)$ is the effective thermal conductivity of a graphene ribbon with width W and length L; Δ is the rootmean-square edge roughness, 0.6 nm;^{11,15} c is a parameter equaling 0.04 W/m/K at 300 K;^{11,15} n is a fitting exponent and λ (L) is the length dependent thermal conductivity for quasi-ballistic transport of wide and short graphene ribbons, which is calculated by a simple model¹⁵ expressed by Eq. (4)

$$\lambda(L) = \frac{G_{\text{ball}}}{A} \left[\frac{1}{L} + \frac{1}{(\pi/2)l_{\text{mfp}}} \right]^{-1},$$
(4)

where G_{ball}/A is the ballistic thermal conductance per unit cross section calculated by Eq. (2) and l_{mfp} is the intrinsic phonon mean free path of large graphene. To obtain the intrinsic phonon mean free path of suspended graphene, we extracted the only two reference data for width dependent thermal conductivity of suspended ribbons ($W = 1.5 \mu m$, $4 \,\mu\text{m}; L = 2.5 \,\mu\text{m}$) from Xu *et al.*¹¹ and reproduced the best fitting using the above empirical model. The reproduced fitting gave the intrinsic mean free path as 214 nm at 300 K, indicating a thermal conductivity of about 1420 W/m/K for large-area suspended graphene sheets, while the intrinsic mean free path is 90 nm for SiO₂-supported graphene at 300 K.¹⁵ Using our present data at 300 K and the intrinsic mean free path of 214 nm, we can obtain the only fitting parameter n as 1.68 for 846 nm long suspended samples, predicting that a wide $(W > 5 \,\mu\text{m})$ and 846 nm long ribbon would have a thermal conductivity of about 1000 W/m/K and that a ribbon narrower than 50 nm would have a thermal conductivity less than 100 W/m/K. However, since the available data are very few, the present prediction for width dependent thermal conductivity needs to be validated by systematic measurements for various sizes in our future work.

IV. CONCLUSION

In conclusion, the existing thermal conductivity data for suspended submicron graphene ribbons are still very few although the thermal conductivity of graphene with submicron sizes is expected to be much smaller than large graphene sheets and strongly size dependent. We measured the temperature dependent thermal conductivity of a suspended graphene ribbon with 169 nm width and 846 nm length using the electrical self-heating method based on the relationship of graphene's electrical resistance and temperature. The measured thermal conductivities range from (12.7 ± 2.95) W/m/K at 80 K to (932 ± 333) W/m/K at 380 K, following $a \sim T^{2.79}$ for the full temperature range of 80 K to 380 K and $a \sim T^{1.23}$ law at low temperatures of 80 K to 130 K. The thermal conductance per unit cross section is only 2.3% of the predicted ballistic limit at 80 K, indicating diffusive phonon transport in this submicron ribbon due to phonon-edge and phonon-defect scattering. Moreover, the present data at 300 K, $(349 \pm 63) \text{ W/m/K}$, were combined with an empirical model to predict possible width dependence of thermal conductivity for 846-nm long suspended graphene ribbons, showing that the thermal conductivity would scale with the width approximately as $\sim W^{1.7}$.

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- ¹E. Pop, V. Varshney, and A. K. Roy, "Thermal properties of graphene: Fundamentals and applications," MRS Bull. **37**, 1273–1281 (2012).
- ²A. A. Balandin, S. Ghosh, W. Bao *et al.*, "Superior thermal conductivity of single-layer graphene," Nano Lett. 8(3), 902–907 (2008).
- ³S. Ghosh, I. Calizo, D. Teweldebrhan, E. P. Pokatilov, D. L. Nika, A. A. Balandin, W. Bao, F. Miao, and C. N. Lau, "Extremely high thermal conductivity of graphene: Prospects for thermal management applications in nanoelectronic circuits," Appl. Phys. Lett. **92**, 151911 (2008).
- ⁴C. Faugeras *et al.*, "Thermal conductivity of graphene in corbino membrane geometry," ACS Nano 4, 1889 (2010).
- ⁵J. U. Lee, D. Yonn, H. Kim *et al.*, "Thermal conductivity of suspended pristine graphene measured by Raman spectroscopy," Phys. Rev. B **83**, 081419 (2011).
- ⁶S. Chen, A. L. Moore, R. S. Ruoff *et al.*, "Raman measurements of thermal transport in suspended monolayer graphene of variable sizes in vacuum and gaseous environments," ACS Nano 5(1), 321–328 (2011).
- ⁷W. Cai *et al.*, "Thermal transport in suspended and supported monolayer graphene grown by chemical vapor deposition," Nano Lett. **10**, 1645–1651 (2010).
- ⁸Q. Y. Li, X. Zhang, and Y. D. Hu, "Laser flash Raman spectroscopy method for thermophysical characterization of 2D nanomaterials," Thermochim. Acta **592**, 67–72 (2014).
- ⁹J. H. Seol, I. Jo, A. L. Moore *et al.*, "Two-dimensional phonon transport in supported graphene," Science **328**, 213–216 (2010).
- ¹⁰X. Xu *et al.*, "Phonon transport in suspended single layer graphene," preprint at arXiv:org/abs/1012.2937 (abstract) and arXiv:org/pdf/1012.2937.pdf (full paper) (2010).
- ¹¹X. Xu *et al.*, "Length-dependent thermal conductivity in suspended singlelayer graphene," Nat. Commun. 5, 3689 (2014).
- ¹²Z. Wang, R. Xie, and C. T. Bui, "Thermal transport in suspended and supported few-layer graphene," Nano Lett. **11**, 113–118 (2011).
- ¹³M. T. Pettes, I. Jo, Z. Yao *et al.*, "Influence of polymeric residue on the thermal conductivity of suspended bilayer graphene," Nano Lett. **11**, 1195–1200 (2011).
- ¹⁴H. Xie, L. Chen, W. Yu *et al.*, "Temperature dependent thermal conductivity of a free-standing graphene nanoribbon," Appl. Phys. Lett. **102**, 111911 (2013).
- ¹⁵M. H. Bae, Z. Li, Z. Aksamija *et al.*, "Ballistic to diffusive crossover of heat flow in graphene ribbons," Nat. Commun. 4, 1734 (2013).
- ¹⁶E. Munoz, J. X. Lu, and B. I. Yakobson, "Ballistic thermal conductance of graphene ribbons," Nano Lett. **10**, 1652 (2010).
- ¹⁷X. Zhang *et al.*, "Thermal and electrical conductivity of a suspended platinum nanofilm," Appl. Phys. Lett. **86**, 171912 (2005).
- ¹⁸M. Fujii, X. Zhang, H. Q. Xie, H. Ago, K. Takahashi, and T. Ikuta, "Measuring the thermal conductivity of a single carbon nanotube," Phys. Rev. Lett. **95**, 065502 (2005).
- ¹⁹C. M. Orofeo, H. Hibino, K. Kawahara, Y. Ogawa, M. Tsuji, K.-i. Ikeda, S. Mizuno, and H. Ago, "Influence of Cu metal on the domain structure and carrier mobility in single-layer graphene," Carbon 50(6), 2189–2196 (2012).
- ²⁰H. Ago, Y. Ito, I. Tanaka, S. Mizuno, and M. Tsuji, "Graphene sheet and method for producing the same," US Patent 8,697,230 B2 (2014).
- ²¹Z. Chen, W. Jang, W. Bao, C. N. Lau, and C. Dames, "Thermal contact resistance between graphene and silicon dioxide," Appl. Phys. Lett. 95, 161910 (2009).
- ²²Y. K. Koh, M. H. Bae, D. G. Cahill, and E. Pop, "Heat conduction across monolayer and few-layer graphenes," Nano Lett. **10**, 4363–4368 (2010).
- ²³N. Mingo and D. A. Broido, "Carbon nanotube ballistic thermal conductance and its limits," Phys. Rev. Lett. 95, 096105 (2005).