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Effect of Pre-treatment Techniques on Physical, Mechanical and Durability Properties of Oriented Strand Board Made from Sentang wood (*Melia excelsa* Jack)

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Sentang wood (Melia excelsa Jack) is one of the promoting fast growing tree species that can be introduced in timber estates and community forest in Indonesia. The objective of this research was to evaluate physical, mechanical and durability of Oriented Strand Board (OSB) made from Sentang wood under various pre-treatment techniques including immersing in hot water, immersing in preservative solution and steamed. Three–layered OSBs were manufactured. The strand composition for face, core, and back was 25%, 50% and 25%, respectively. Methane di-isocyanate (MDI, Type H3M) resin was used as an adhesive in amount of 7%. The amount of paraffin used was 1% based on oven dried strand. The strands were immersed in hot water at 80 °C for 2 hours, immersed in 2.5% of CCB preservative solution for 48 hours and steamed at 126 °C at 1.4 kg.cm⁻² pressure for 1 hour prior to be blended with adhesive. The results indicated that OSB manufactured mostly consisted of quarter round and flat strands with high slenderness ratio and high aspect ratio. Pre-treatment of strand by immersing strands in hot water, immersing in preservative solution and steamed resulted in improvement of water absorption of board, some mechanical properties and durability of OSB. Introducing 2.5% CCB preservative on the OSB significantly improved durability of OSB against termite attack but did not influence the strength of OSB. Untreated OSB, OSBs prepared from preserved strands and steamed strands can be used for exterior application, while OSB prepared from hot water immersed strands only can be used for interior application. All OSB parameters manufactured in this experiment were superior when compared with the minimum requirement of CSA 0437.0 standard for Grade O-2 OSB.

INTRODUCTION

The trend of wood supply from natural forests for wood industries in Indonesia showed sharply decreased in the last decade. On the other hand, due to the lack of wood supply as raw materials for wood industries in Indonesia, the cost of wood occupied about 60~65% of the product price (BRIK, 2007). It was reported that up to the first quarter 2008, the total areas of timber estates developed in Indonesia are around 3.032 million hectares (Ministry of Forestry of Indonesia, 2008). It is predicted that in near future the supply of wood from timber estates and community forests will play a dominant role in substituting the wood supply from natural forests in Indonesia. Unfortunately, most of the wood extracted from community forests belong to the lower quarified

wood than those with medium density with small diameter and wide variety in species. It also contains a lot of natural defect (i.e, checks, knots etc) and has a low dimensional stabilization and low natural durability. Hence, the types of wood are not suitable for solid wood, but very promising as raw materials for wood composites product.

Oriented strand board (OSB) is a structural panel suitable for a wide range of construction and industrial applications. It is a mat-formed panel made of strands sliced in the long direction from small diameter, fast growing round wood logs and bonded with an exterior-type binder under heat and pressure (Structural Board Association, 2005). OSB was manufactured in a cross-oriented pattern similar to plywood to create a strong, stiff structural panel (APA, 2009). OSB is composed of thin rectangular-shaped wood strand arranges in layers at right angles to one another, which are laid up into mats that form a panel. OSB is bonded with fully waterproof adhesive.

Sentang wood (*Melia excelsa* Jack) is one of the promising fast growing tree species that can be introduced in timber estates and community forest. *M. excelsa* has a medium fiber length and a lumen diameter, where as the fiber diameter and cell wall thickness are categorized to the thin~medium. *M. excelsa* also has a small pore diameter, and therefore it is predicted that this wood belongs to a low permeability wood. The tangential, radial and longitudinal shrinkages rates of *M. excelsa* are 5.0%, 4.3%, and 1.80 %, respectively. *M excelsa* wood has a bulk density around 0.42–0.52 to be catego-

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rized as a medium density wood. This wood has a low compression strength and a medium~low bending strength. $M.\ excelsa$ belongs to non durable wood based on grave yard test performance (Iswanto, 2008). The extractive content of $M.\ excelsa$ after dissolved in cold water, hot water, 1% sodium hydroxide (NaOH 1%) and alcohol—benzene were in the range of $4.25\sim5.07\%$, $7.39\sim7.83\%$, $9.29\sim11.19\%$, and $2.09\sim2.64\%$, respectively (Iswanto, 2008). Based on the above information $M.\ excelsa$ wood can be used for light construction, furniture, panel and veneer. Hence, $M.\ excelsa$ wood is also promising to be used as a raw material for OSB product.

In order to open passways for usage of the above wood, the objective of this research was to evaluate the effect of pre-treatment techniques (i.e., immersing in hot water, preservative solution and steamed) on physical, mechanical and durability properties of OSB made from Sentang wood (*M. excelsa*).

MATERIALS AND METHODS

Materials

 $M.\ excelsa$ wood was collected from Arboretum of Faculty of Forestry, Bogor Agricultural University, Bogor, Indonesia. The strands were produced by using disk flaker. The size of strand used was $60{\sim}70\,\mathrm{mm}$ (I), $28{\sim}30\,\mathrm{mm}$ (w), and $0.6{\sim}0.7\,\mathrm{mm}$ (t). Commercial Methane di–isocyanate (MDI, Type H3M) as an adhesive was used to bind the strands. The amount of MDI adhesive and paraffin used were 7% and 1% based on oven dry (OD) weight of strand, respectively. Chromate–copper–boron (CCB) preservative was used in amount of 2.5%. The moisture content (MC) of strand was 7%.

Strand manufacturing

To set the strand width, the wood materials were cut into planks with dimensions of $2,000\times25\,\mathrm{mm}$ in length and thickness by using band saw. To set the strand length, planks were cut into small blocks with dimensions of $70\times25\,\mathrm{mm}$ in length and thickness by using circular saw. The disk–flaker used to manufacture the strands determined the thickness of the strands. The thickness depended on the width of the gap between the cutting knife and the disc.

Treatment of strands

A part of strands was immersed in hot water at 80 °C for 2 hours, immersed in 2.5% CCB preservative solution for 48 hours, and steamed in an autoclave at 126°C at $1.4\,\mathrm{kg/cm^2}$ for 1 hour. Then, the strands were dried in the oven at 75~80 °C for several days to reach about 3% of the MC. For comparison, untreated strands were also prepared.

Manufacturing of OSB

Three layered OSB were produced with the size of 30 by 30 by $0.9~\rm cm^3$ and the target density was $0.7~\rm g/cm^3$. The OSB layers were hand—made with face and back layers aligned perpendicular to the core layer. The weight ratio of the face—to—core—to—back layers were set at

1:2:1. Rotary drum blender was used for mixing strand, adhesive and paraffin. After the mat was hot–pressed at $160\,^{\circ}\text{C}$ under $25\,\text{kg/cm^2}$ as the pressure for $6\,\text{min}$, the board was conditioned for three weeks in a room adjusted in the range of $25{\sim}30\,^{\circ}\text{C}$ and $60{\sim}65\%$. Three boards were prepared for each treatment.

Determination of physical and mechanical properties

Prior to physical, mechanical and durability against termite attack tests, specimens were conditioned for 7 days in a room adjusted at 25~30 °C. The board parameters measured were air-dry density, MC, water absorption (WA), thickness swelling (TS), linear expansion (LE), modulus of rupture (MOR) and modulus of elasticity (MOE) in bending, and internal bond (IB). The dimension of specimens for evaluation in air-dry density and MC of boards is 100 by 100 by 9 mm³. The specimens were weighed immediately after dried in the oven at 103±2 °C until they reached constant weight. For WA, TS and LE tests, the dimension of specimens is 50 by 50 by 9 mm³. The specimens were also weighed immediately. Average thickness was determined by taking several measurements at specific locations. After 24 hours of submersion, specimens were dripped and wiped for cleaning of any surface water, the weight and thickness of specimens were measured. Mechanical properties (MOE, MOR, and IB) were tested by using universal testing machine (UTM) equipped with a load cell with a capacity of 10,000 N. The dimension of specimens in bending tests is 200 by 50 by 9 mm³. MOE and MOR were measured both in dry and wet states in their long dimension parallel to the major axis of panel. While for IB test, the dimension of specimens is 50 by 50 by 9 mm³. Evaluation of MOE, MOR, and IB parameters were per-

Table 1. Resistance level of wood against termite attacked based on Antifeedant classification

Class	Antifeedant value (%)	Resistance level
IV	$75 \le x < 100$	very strong
Ш	$50 \le x < 75$	strong
${ m II}$	$25 \le x < 50$	moderately strong
I	$0 \le x < 25$	weak

Source: Sornnuwat et al. (1995)

Table 2. Resistance level of wood against termite attacked based on termite mortality

Mortality (%)	Resistance level			
≥95	very strong			
$75 \le x < 95$	strong			
$60 \le x < 75$	fairly strong			
$40 \le x < 60$	moderately strong			
$25 \le x < 40$	fairly weak			
$5 \le x < 25$	weak			
< 5	in-active			

Source: Sornnuwat $et\ al.\ (1995)$

formed at 28 $^{\circ}\mathrm{C}$ and 60% R.H. The crosshead speed was adjusted at 10.00 mm/min.

The resistance of OSB against subterranean termite (Coptotermes curvignathus Holmgren) attack.

The resistance of OSB against subterranean termite ($C.\ curvignathus$) attack was determined through a modified wood block test. Samples with the dimension of 20 by 20 by $10\ \mathrm{mm^3}\ (l\times w\times t)$ were exposured for 4 weeks to termites in order to obtain weight loss, antifeedant and termite mortality parameters. Before and after the tests, the samples were dried in the oven at $103\pm2\ ^\circ\mathrm{C}$ for determining of weight loss and antifeedant. Antifeedant was determined by calculating the ratio between weight loss of untreated and treated samples. Table 1 and 2 showed the resistance level of wood against termite attack based on antifeedant and mortality classification.

Analysis

For physical and mechanical properties, all multiple comparisons were subjected to an analysis of variance (ANOVA). Highly significant ($\alpha \le 0.01$) and significant ($\alpha \le 0.05$) differences between mean values of the untreated and treated specimens were determined using Duncan's multiple range tests.

RESULTS AND DISCUSSION

Strand geometry and curling

Strand geometry is a prime parameter affecting both board properties and its manufacturing process. Suchsland and Woodson (1991) suggested that strand geometry is of greater significance in the development of board properties than the actual mechanical properties of the fibers themselves. It has a definite relationship with the compression ratio, and thus it will influence the density of the composite board. The slenderness and aspect ratios were calculated based on the ratio of strand length to strand thickness and strand length to strand width, respectively (Maloney, 1993).

The mean values of length, width, thickness, slenderness ratios and aspect ratios of the strands and their distribution used in this study are presented in Table 3, Fig. 1 and Fig. 2. The respective mean values obtained in this experiment were 70.52 mm in length, 23.68 mm in width and 0.87 mm in thickness, yielded slenderness ratio 85.59 and aspect ratio 2.99. The slenderness of strands produced was varied from 55.06 to 108.12. The higher the slenderness ratios resulted in the better contact area

 $\textbf{Table 3.} \ \text{Dimension, slenderness ratio and aspect ratio of strand}$

Parameter	Average	Minimum	Maximum
Length (mm)	70.5 ± 1.0	64.1	71.7
Width (mm)	23.7 ± 1.1	21.4	25.3
Thickness (mm)	0.9 ± 0.2	0.3	1.2
Slenderness	85.6±23.3	55.1	108.1
Aspect ratio	2.9 ± 0.1	2.7	3.4

n: 100 strands

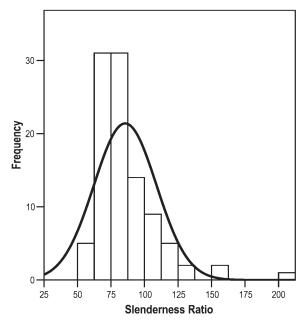


Fig. 1. Distribution of strand slenderness ratios of Sentang wood (*M. excelsa*).

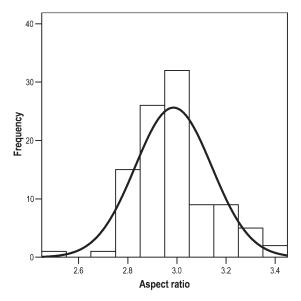


Fig. 2. Distribution of strand aspect ratios of Sentang wood (*M. excelsa*).

in the mat, the better mechanical properties of finished board and less consumption of binder in the board (Moslemi, 1974) were provided. The strands aspect ratio ranged from 2.73 to 3.43 in which all ratios were above 2. A particle cannot be oriented if having aspect ratio of one (square shape). Maloney (1993) stated that wood strands having an aspect ratio greater than one are easily oriented during forming process. According to Shuler *et al.* (1976) and Kuklewski *et al.* (1985), a strand aspect ratio of two is enough to produce OSB with superior properties. The results showed that the strands of *M. excelsa* yielded a high slenderness ratio and a high aspect ratio.

Characteristics of strand curling were listed in Table 4. The results showed that strand thickness significantly 374 A. H. ISWANTO et al.

Table 4. The curliness of strand

Class	Strand (%)	Length (mm)	Width (mm)	Thickness (mm)	
1. Flat	33	70.5	23.6	0.9	
2. Curl, quarter round	55	70.5	23.7	0.8	
3. Curl, half round	12	70.4	23.6	0.7	

n: 100 strands

affected the curling of strand, while the strand length and width showed no significant effects. The thicker strand tends to be more flat when compared with the thin one which tends to curl up easier. OSBs manufactured in this experiment mostly consisted of quarter round strands and flat strands which are suitable to manufacture OSB panels. Strand shape for OSB manufacture should be rectangular, thin, long and narrow. Ideal strand should also be straight and flat without curling, because a higher curling of strands can bring the same trouble in the adhesion between strand and adhesive, which could also affected on board properties manufactured (Maloney, 1993). A study by Misran (2005) suggested that rubber wood strands tended to curl when it was produced by using disk flaker. A similar problem was encountered in this study where the strands were found to warp on one side of its surface.

Properties of OSB made from Sentang wood (Melia excelsa Jack) under various pre-treatments techniques

M. excelsa belongs to non durable wood and contains a relatively high amount of extractives (Iswanto, 2008). In order to improve quality of the final product of OSB, the evaluation of the physical properties (i.e., density, MC, WA, TS, and LE) and mechanical properties (i.e., MOR, MOE, and IB) of OSB made from M. excelsa together with its resistance against subterranean termite (C. Curvignathus) attack (i.e., weight loss, antifeedant and mortality) were conducted under various pre–treatment techniques, namely immersing in hot water, immersing in preservative solution and steamed.

Physical properties of OSB

The mean values of air—dried density and MC of OSB were varied between 0.58 to 0.60 g/cm³, and 8.59 to 11.80%, respectively. The air—dried density obtained in this experiment was lower than the target density of 0.70 g/cm³ (Table 6). It was due to a spring back of the board during pressing and swelling in the board conditioning. After pressing, the resulted board thickness exceeded the thickness target of 9.00 mm. The lowest and the highest MC values were provided from OSBs prepared from hot water immersed strands and untreated strands, respectively. However, a statistical analysis showed that all pre—treatments for strands adopted in this experiment do not significantly affect the air—dried density and MC parameters.

The mean values of WA, TS and LE after immersing in cold water for 24 hours were varied between 22.30 to 42.24%, 6.89 to 7.63%, and 0.85 to 1.04%, respectively

(Table 6). The lowest and the highest WA values were obtained on OSBs prepared from preserved strands and untreated strands, respectively. The similar phenomenon occurred the parameter. On the other hand, the lowest and highest values of TS were obtained by OSBs prepared from steamed strands and untreated strands, respectively. The strand pretreatment had a significant effect on the WA parameter, whereas the TS and LE parameters were not significantly affected by the strand pre–treatment.

Pre-treatment of strands by immersing in hot water, preservative solution and steamed decreased the WA value of OSB. It was presumably due to some extractives removed during the pre-treatment of strands. Extractives can cause poor water resistance properties of the finished products (Maloney, 1993). Furthermore, MDI resin is very sensitive to wood extractives. The value of extractives of M. excelsa dissolved in cold water and hot water are varied in the range of 4.25~5.07%; respectively (Iswanto, 2008). Pre-treatment of strands by steam improved the WA value, which agreed with the result of Rowell et al. (2002) that had prepared fiberboard from steamed fibers. It is also interesting to note that the treatment of strands with preservative solution gave a positive effect on dimensional stability of OSB prepared from M. excelsa. Although CSA 0437.0 standard for Grade O-2 OSB (SBA, 2004) dose not require WA and LE parameters, all the TS values obtained in this experiment met the requirement of CSA 0437.0 standard for Grade O-2 OSB (SBA, 2004).

Mechanical properties of boards

The mean values of MOR in parallel to the grain direction of OSB both in dry and wet states were 39 MPa and 18 MPa; 61 MPa and 6 MPa; 34 MPa and 16 MPa; and 44 MPa and 20 MPa, respectively for untreated, hot water immersed, immersed in preservative solution, and steamed boards, as listed in Table 6. The highest and the lowest values of MOR in the dried state condition were achieved on boards prepared from strands immersed in hot water and boards prepared from preserved strands respectively. The highest and the lowest values of MOR in the wet condition were achieved on steamed boards and boards immersed in hot water, respectively. Furthermore, the mean values of MOE of the same specimens were 4,460 MPa and 1,900 MPa; 6,460 MPa and 960 MPa; 5,500 MPa and 2,050 MPa; and 6,010 MPa and 2,510 MPa, respectively for untreated, hot water immersed, immersed in preservative solution and steamed boards, also as listed in Table 6. The highest and the lowest values of MOE in the dry state condition were achieved on boards prepared from hot water immersed strands and untreated strands, respectively. The highest and the lowest values of MOE in the wet condition were achieved on steamed boards and hot water immersed boards, respectively.

It is clear that the pre—treatment of strands in hot water at 80 °C for 2 hour significantly improved the MOR and MOE values in the dry state condition. The results also indicated that a control board, boards prepared

from preserved strands and boards prepared from steam strands have similar values of MOR and MOE in the dry state condition. However, boards prepared from steam strands tend to result in higher values of MOR and MOE. Boards prepared from preserved strands tend to result in a higher value of MOE (Table 6). However, when bending strength was measured in the wet state condition, the MOR and MOE values of boards prepared from hot water immersed strands were lower than 3 other treatments (i.e., untreated, immersed in preservative solution and steamed boards). Among others, boards prepared from steam strands showed a superior bending strength in the wet condition.

Extractives are not a part of the wood structure. They include tannins and other polyphenolics, coloring matters, essential oils, fats, resins, waxes, gums, starch, and simple metabolic intermediates (Maloney, 1993). They can be removed by use of appropriate solvents. The extractives cause some problems in particleboard manufacturing i.e., consumption of resin and its curing rate, poor water resistance properties of the finished products, and a blow problem during the pressing. It is known that immersing the strands in cold and hot water dissolved such wood extractives. The presence of the extractives can block the adhesive penetration into the wood particles, resulting in the lower mechanical properties of particle boards achieved (Maloney, 1993). Immersing the strands in hot water can provide an improvement of the surface tension of strands and the adhesion of strands and adhesives (Alamsyah, et al., 2008). Thus, it can also improve the strength of the composite. It was reported that the strength of OSB prepared from Acacia mangium wood strands and flake boards prepared from red meranti wood flakes (Shorea leprosula) was much improved after the strands/particles were immersed in hot water for 2 hours (Febrianto $et\ al.$, 2009; Hadi, 1988). Furthermore, heat treatments on wood particles could cause a decrease in acidic degrees of wood by forming acetic acid and formic acid. The acids hydrolyzed celluloses and hemicelluloses result in reducing of mechanical properties (Boonstra $et\ al$; 2006). In fact, we observed that delamination occurred on the OSB prepared from hot water immersed strands after they were immersed in cold water prior to be tested in the wet condition.

Strength retention is defined as a ratio between MOR or MOE in a wet state to MOR or MOE in a dry condition. The higher the strength retention value, the more suitable the board for exterior application (Massijaya and Okuma, 1996). Table 6 also exhibits the strength retention of OSB prepared under various pre-treatment techniques. Based on the strength retention value obtained in this experiment, it can be said that untreated OSB and OSB prepared from preserved and steamed strands can be used under severe condition considering exterior application. Although OSB prepared from hot water immersed strands had the most superior value of MOR and MOE in the dry condition, this type of OSB can only be used for structural interior application. Nuryawan et al. (2008) reported that OSB made from untreated strands of Acacia mangium, Eucalyptus sp. and Gmelina arborea bonded with MDI resin can be used for exterior application.

The mean values of IB of OSB prepared from untreated, hot water immersed, immersed in preservative solution and steamed strands were 0.5, 0.9, 0.5, and 1.9 MPa, respectively. The highest and the lowest values of IB were achieved on boards prepared from steamed strands and preserved strands, respectively. The pretreatment of strands by steam prior to board manufac-

Table 5.	Resistance of	OSB against	termite	аттаск ра	ised on antii	eedant and termite mortality
				4	1 (0/2	

Treatment	Weight loss (%)	Antifee	dant (%)	M	Mortality (%)		
Control	7.5	_	(weak)	40.0	(moderately strong)		
Hot Water Immersed	5.5	15.4	(strong)	64.6	(fairly strong)		
Preservative Solution	0.6	85.1	(weak)	100.0	(very strong)		
Steamed	8.9	8.1	(weak)	52.0	(moderately strong)		

Table 6. Effect of Pre-Treatment Techniques on Physical and Mechanical Properties of OSB Prepared from Sentang wood (M. excelsa Jack)

Treatment	WA 24H (%)		LE 24H (%)	MOR (MPa)		MOE (MPa)		Strength Retention (%)		IB (MPa)
	(/0)		(,0)	Dry	Wet	Dry	Wet	MOR	MOE	
Untreated	42.24±5.56°	7.63±2.04	0.92±0.21	39±10°	18±4 ^b	4460±590°	1900±210 ^b	46.27±3.31	42.68±0.86	0.5 ± 0.1^{a}
HWI	28.51 ± 2.94 ab	7.46 ± 1.06	1.04 ± 0.06	$61 \pm 11^{\rm b}$	6 ± 1^{a}	$6460 \pm 490^{\circ}$	960 ± 100^{a}	9.95 ± 1.27	14.64 ± 2.79	0.9 ± 0.3^{a}
PSI	22.30±2.92ª	7.02 ± 1.64	0.85 ± 0.15	34 ± 10^{a}	$16\pm 2^{\rm b}$	5500 ± 760^{ab}	$2050 \pm 110^{\rm b}$	49.78±12.54	37.84±6.93	0.5 ± 0.1^{a}
Steam	$32.45 \pm 2.11^{\text{b}}$	6.89 ± 0.51	0.93 ± 0.08	$44\pm7^{\mathrm{ab}}$	$20 \pm 2^{\rm b}$	6010 ± 1270^{ab}	$2510 \pm 190^{\circ}$	47.01 ± 9.68	43.15 ± 10.52	$1.9 \pm 0.2^{\rm b}$
CSA 0437.0 (Grade O-2) standard	N/A	≤ 15	N/A	296	N/A	56084	N/A	N/A	N/A	3.52

Notes: HWI: Hot water immersed; PSI: Preservative solution immersed; Homogeneity group: Same letters in each columns indicated that there is no significant difference between the samples according to the Duncan's multiple range test. p: 0.01.

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turing improved the IB value significantly. The IB value of OSB prepared from steamed strands was about 2~4 times higher than those of OSBs prepared from preserved strands, untreated strands and hot water immersed strands. In the steam treatment, free sugars in wood particles were converted into furan intermediates. Then, furan intermediates can be converted into furan resin, resulting in improvement in IB values and dimensional stability of board. This result agreed with the previous result of fiberboards prepared from steamed fibers reported by Rowell et al. (2002).

Almost all mechanical parameters of OSB except MOE of untreated boards prepared in this experiment were higher than the minimum requirement in the properties according to CSA 0437.0 standard for Grade O–2 OSB (SBA, 2004).

The resistance of OSB against subterranean termite (Coptotermes curvignathus Holmgren) attack

Subterranean termite gives the worst damage in wood and wood products deterioration in the tropical region. Subterranean termite utilizes wood both as a shelter and food sources. As *M. excelsa* wood belongs to non durable wood (Iswanto, 2008), the resistance of OSB from M.excelsa strands against subterranean termite (*C. curvignathus*) attack under various pre–treatment techniques was observed.

The mean value of weight loss of samples after baited for 4 weeks to subterranean termite (C. Curvignathus) ranged between 0.61~8.90%. The lowest and the highest values of the weight loss were achieved on OSB prepared from preserved strands and steamed strands, respectively (Table 5). Based on the antifeedant criteria, the untreated, hot water immersed and steamed treatments showed a similar resistance to subterranean termite (C. Curvignathus), indicating weak or less resistance. On the other hand, OSB prepared from preserved strands exhibited a strong resistance to subterranean termite (C. Curvignathus). An almost similar phenomenon occured when the resistance of OSB was measured based on the termite mortality criteria. The lowest and the highest termite mortality were obtained on OSB prepared from the untreated and preserved strands, respec-The untreated board, boards prepared from steamed strands were categorized to moderately strong, while OSB prepared from hot water immersed strands and preserved strands were categorized to fairly strong and very strong resistance to subterranean termite (C. Curvignathus) under the adopted experimental condi-

CONCLUSIONS

OSB manufactured mostly consisted of quarter round and flat strands with a high slenderness ratio and a high aspect ratio. The pre-treatments of strands by immersing strands in hot water, immersing in preservative solution and steamed improved water absorption of OSB and some mechanical properties in addition to durability of OSB. OSB prepared from hot water immersed strands

has very excellent physical and mechanical properties in a dry state condition, but it provided a very low strength retention value. OSB prepared from steamed strands had excellent physical and mechanical properties both in the dry and wet states. OSB prepared from preserved strands had the same quality as the untreated OSB in terms of physical and mechanical properties, but it showed a strong resistance against termite attack. Therefore, untreated OSB, OSB's prepared from preserved strands and steamed strands can be used for exterior application, while OSB prepared from hot water immersed strands only can be used for interior application.

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