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Resistivity Imaging by CSAMT Method in Takigami Geothermal Field in Kyushu, Japan

by

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Abstract

Controlled-source audiofrequency magnetotelluric (CSAMT) survey was carried out in Takigami geothermal field. Stations were taken closely with regular grid spacing of 150 m. The purpose of the measurements is to delineate a detailed resistivity structure and location of electrical discontinuities that may reflect a possible faults and fractures correlated with a promising reservoir. Although the CSAMT measurements were conducted at a distance of 6 km away from a transmitter, the CSAMT data still contain some near field data when the frequency from transmitter signal is low range. Therefore, before applying two-dimensional (2-D) magnetotelluric (MT) inversion analysis of transverse magnetic (TM) mode, data corrections for a near field and transition zone were made. The interpretation results based on 2-D inversion show that there are some electrical discontinuities found in the N-S and W-E directions, which correlate with the trend of some faults where the geothermal reservoir may exist. The electrical discontinuity F_d in N-S direction correlates with the Noine fault zone, which divides the subsurface into eastern and western parts according to the characteristics of electrical resistivity, permeability, temperature, and reservoir depth. The electrical discontinuity F_a in W-E direction corresponds to the Teradoko fault where the major production wells have been drilled in the area.

Keywords: CSAMT, 2-D inversion, Geothermal reservoir, Takigami area

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1. Introduction

Signal of magnetotelluric (MT) method is considered to be due to thunderstorms and solar winds in ionosphere for which the field strength and polarization vary with time of day and season. To improve the signal strength problem of the MT method, Goldstein and Strangway¹⁾ developed the audiofrequency MT technique with a grounded electric dipole as an artificial source called controlled-source audiofrequency magnetotelluric (CSAMT). Over the years, CSAMT has emerged as a powerful exploration tool and has found its application in a mineral exploration²⁾, geothermal investigation^{3,4)} and a potential radioactive waste disposal characterization⁵⁾. An excellent review of CSAMT and its application is given by Zonge and Hughes⁶⁾. The advantages of this technique operated with MT method are that the polarization of the fields can be selected by the orientation of the transmitting antenna and the signal strengths do not depend on the time of day or season. However in the CSAMT method, the non-plane wave nature of the source limits the interpretation of the data. Recognizing this, the CSAMT measurement must be carried out at a distance greater than 3-5 skin depths from the transmitter site where the plane wave approximation is valid. Mustopa et al.⁷⁾ have interpreted the MT data in the Takigami geothermal field to determine the subsurface resistivity structure correlated to the promising reservoir zone and distribution of fault systems and trends. However, the stations of MT measurements are not in closely and regularly spaced. Accordingly, the MT data interpretation results do not sufficiently represent a full resistivity imaging reflected from the subsurface in the area.

The CSAMT measurements, in the operating frequency range of 0.167 Hz to 1024 Hz, and one-dimensional (1-D) inversion of MT analysis have been carried out by West Japan Engineering Consultants⁸⁾ under the project of Idemitsu Geothermal Co. in the Takigami geothermal field, central Kyushu, Japan (**Fig. 1**). The CSAMT measurements were carried out in more closely and regular grid spacing station (150 m) than that in the MT measure-

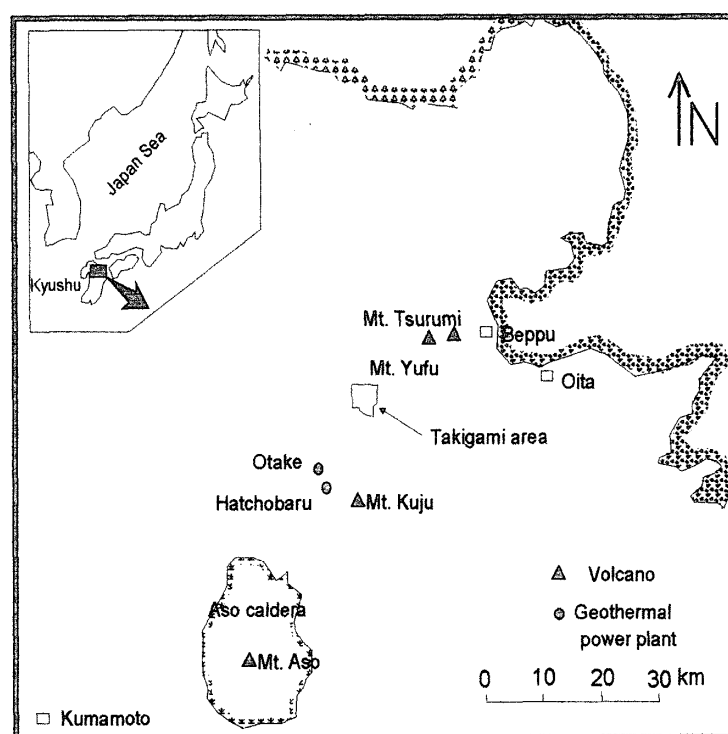


Fig. 1 Northern Kyushu with the location of Takigami area.

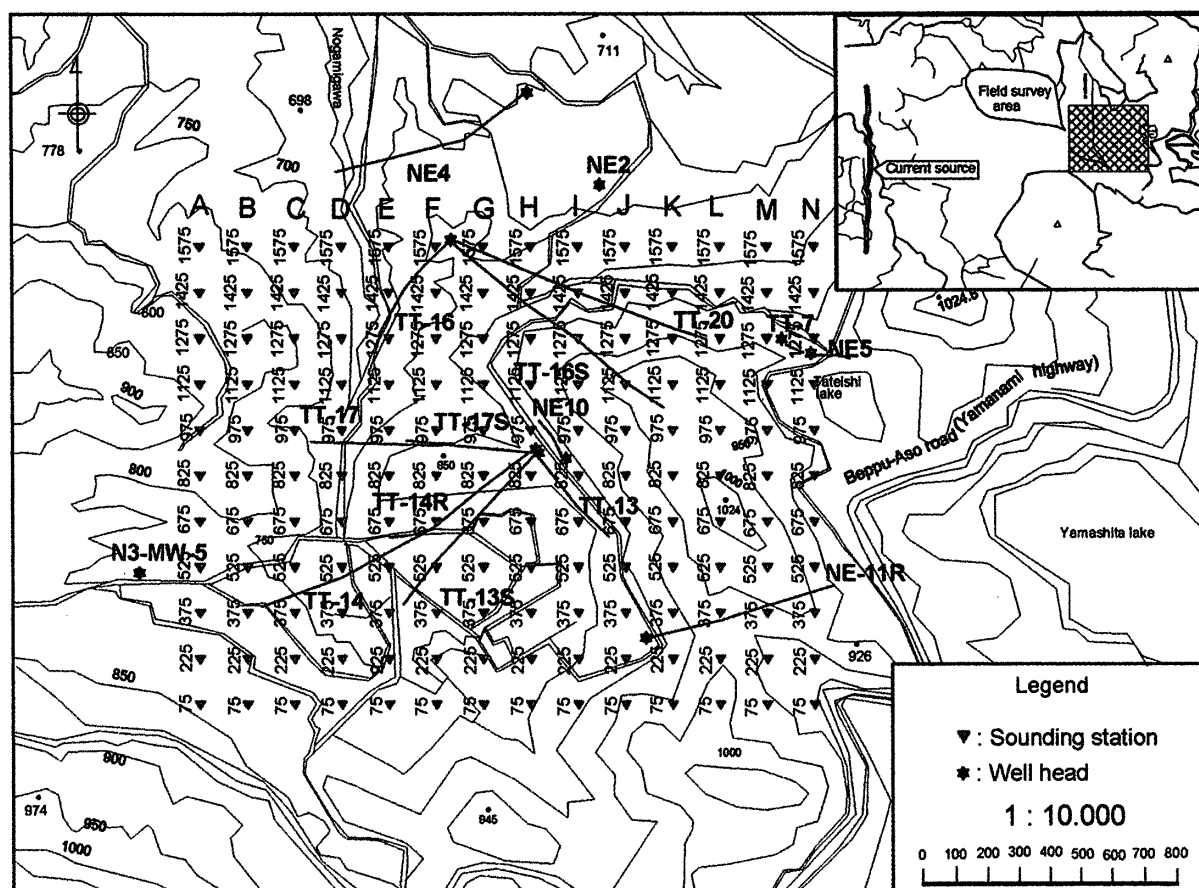


Fig. 2 The location map of CSAMT measurements in Takigami area.

ments as shown in Fig. 2. Since measurements were made using the electric field along the transverse, we assumed that the data correspond to the transverse magnetic (TM) mode⁹⁾. Although the CSAMT measurements were carried out at the sites about 6 km away from the transmitter to maintain plane-wave assumption, the CSAMT data still contain some near field effect when the frequency from transmitter signal is low (deep survey). Therefore, it needs correction for a near-field effect before applying the MT interpretation technique.

1-D inversion of MT data is good procedure when a regional structure is approximately horizontal, as in a sedimentary basin. However, when the structure is not approximately layered, the 1-D inversion technique is not valid. To overcome the problem, 2-D inversion procedure is an essential tool to interpret the MT data. In this paper we applied a 2-D inversion of MT data based on a non-linear conjugate gradient method¹⁰⁾ for the CSAMT data in Takigami geothermal field.

2. Geological setting

The Takigami area is located on the gentle western slope of Mt. Noine at the elevation of about 700 m and included to the Hoho geothermal region, which is one of the most active geothermal fields in Japan. The Hoho geothermal region has an outstanding level of geothermal resources, with many volcanoes and geothermal manifestation such as hot springs, fumaroles and hydrothermal alteration halos at the surface. Although the Takigami area lies in the promising Hoho geothermal region, there are no surface geothermal manifestations in the immediate area. More than 20 exploration wells have been drilled in the field since 1981. As the results, the geothermal reservoir with high temperature was detected,

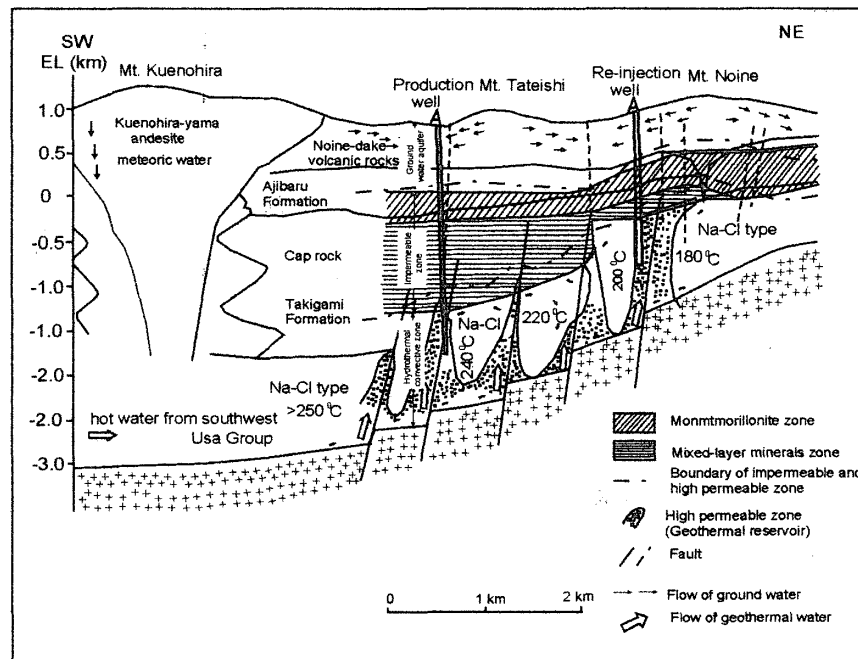


Fig. 3 Schematic cross-sectional geologic model of Takigami geothermal system.

which is covered with the thick impermeable layer. The maximum temperature of the reservoir is 252°C ¹¹⁾. The subsurface model of the area (**Fig. 3**) is divided into three parts^{12,13)}. The upper layer, which is composed of Quaternary Noine-dake volcanic rocks, Kusu and Ajibaru formation, shows low thermal gradient and low temperature below 50°C . The middle layer, which is composed of Tertiary dacitic and andesitic volcanics called Takigami formation, shows high thermal gradient. The lower layer, which is composed of Tertiary andesitic and dacitic rocks called Usa group, shows isothermal gradient and high temperature ($160 - 260^{\circ}\text{C}$) where this layer is the geothermal reservoir of the field.

According to reservoir characteristics, the reservoir of Takigami geothermal field is divided regionally into two parts, that is, eastern and western¹⁴⁾. There are significant differences in terms of subsurface temperature distributions, depth of fractured reservoirs, and permeabilities. The boundary is probably the Noine fault zone. The eastern part of the reservoir system is shallow ($700 - 1100$ m depth), high permeability ($30 - 100$ darcy-m) and has the temperature ranges from 160 to 210°C . On the other hand, the western part of reservoir is deeper ($1500 - 2000$ m depth), low permeability ($5 - 30$ darcy-m) and high temperature ($230 - 250^{\circ}\text{C}$). This two-part reservoir accounts for the difference in chemical composition of the geothermal fluid, and the variation in the hydrology and thermal structure of the system. The present subsurface fluid flow pattern in the area has been analyzed by using distributions of geothermal indicators, such as lithium concentration, chloride-lithium and sodium-potassium ratio. As the result the lithium concentration in the reservoir fluids decrease from southwest to the north, indicating that temperature decrease in the same direction. It means the fluids flow toward the north and northeast (shallower part) from the southwest (deeper part) where is no evidence for deep mixing with the cold surface ground water. Then the production and reinjection wells were drilled in the southwestern and the northeastern part, respectively. The most adequate capacity (about 70% of steam) of the production was estimated at 55 MW of power generation¹⁵⁾.

3. CSAMT theory

Basic principle for CSAMT theory can be described in terms of Maxwell's equations. Since CSAMT measurements employ a grounded electric dipole, in a source free region, the electric and magnetic field can be decomposed in terms of Schelkunoff potential A and F ¹⁶⁾,

$$E = -\nabla \times zF_z(x, y, x, \omega) - (i\omega\mu)(zA_z) + \frac{1}{(\sigma + i\omega\epsilon)}\nabla(\nabla \cdot zA_z) \quad (1)$$

$$H = \nabla \times zA_z(x, y, x, \omega) - (\sigma + i\omega\epsilon)(zF_z) + \frac{1}{i\omega\mu}\nabla(\nabla \cdot zF_z) \quad (2)$$

where E is the electric field intensity, H is the magnetic field intensity, z is the unit vector in the vertical direction, σ is the electrical conductivity, ϵ is the electrical permittivity, μ is the magnetic permeability, and ω is the angular frequency.

The general solutions of a tangential component of electric field (E_ϕ) and a radial component of magnetic field (H_r) from equations (1) and (2) are expressed in cylindrical coordinates¹⁷⁾ as

$$E_\phi = \frac{Idl \sin \phi}{2\pi\sigma r^3} [2 - e^{-ikr}(1 + ikr)] \quad (3)$$

$$H_r = \frac{Idl \sin \phi}{2\pi r^2} \left\{ 3I_1\left(\frac{ikr}{2}\right)K_1\left(\frac{ikr}{2}\right) + \frac{ikr}{2} \left[I_1\left(\frac{ikr}{2}\right)K_0\left(\frac{ikr}{2}\right) - I_0\left(\frac{ikr}{2}\right)K_1\left(\frac{ikr}{2}\right) \right] \right\} \quad (4)$$

where dl is the dipole length, r is the source-sounding distance, and I_m and K_m are modified Bessel function of the m -th order.

From equations (3) and (4), it is evident that the relative strengths of these components are dependent upon r , media properties and frequencies. Media properties and frequency determine the skin depth δ . We can visualize the functional dependence of equations (3) and (4) as the ratio of r to δ , that is

$$|kr| = \frac{(r\sqrt{2})}{\delta} \approx \frac{r}{\delta} \quad (5)$$

where $|kr|$ is commonly referred to as the induction number.

According to the characterization of the induction number, there are three regions of propagating electromagnetic (EM) field in CSAMT method. The region near the transmitting dipole is electrically characterized by small induction ($|kr| \ll 1$) known as “near-field” zone. The region far from transmitting dipole is electrically characterized by large induction number ($|kr| \gg 1$) known as “far-field” or “plane-wave” zone. The region between these zones is called “transition” zone.

3.1 Near-field response ($|kr| \ll 1$)

The equations (3) and (4) can be determined by using the appropriate approximations for the complex Bessel functions and exponentials. The results are:

$$E_\phi \approx \frac{Idl \sin \phi}{2\pi\sigma r^3} \quad (6)$$

$$H_r \approx \frac{Idl \sin \phi}{4\pi r^2} \quad (7)$$

From the equations (6) and (7), E is directly proportional to ground resistivity and independent of frequency. H is independent of both resistivity and frequency (saturated). The near-field apparent resistivity is a function of r , that is

$$\rho_a \approx \frac{r}{2} \left| \frac{E_\phi}{H_r} \right| \quad (8)$$

This shows that near-field measurement and depth penetration are controlled by array geometry, not by frequency.

3.2 Far-field response ($|kr| \gg 1$)

Far from dipole source, equations (3) and (4) approach the following limits, with quasi-static assumption,

$$E_\phi \approx \frac{Idl \sin \phi}{\pi \sigma r^3} \quad (9)$$

$$H_r \approx \frac{Idl \sin \phi}{\pi \sqrt{\mu \sigma \omega} r^3} e^{-\frac{i\pi}{4}} \quad (10)$$

For a homogenous earth, the E -field is independent of frequency and directly proportional to resistivity. The horizontal H -field components are frequency-dependent and a function of the square root of ground resistivity. Hence H does not “saturate”, and it is fully responsive to resistivity change and frequency.

As shown in equations (9) and (10) the horizontal fields in the far-field zone all decay as $1/r^3$, thus the far-field apparent resistivity can be determined by measuring the perpendicular E and H , that is

$$\rho_a = \frac{1}{\mu \omega} \left| \frac{E_\phi}{H_r} \right|^2 \quad (11)$$

which is commonly called the Cagniard resistivity (MT apparent resistivity).

3.3 Transition zone ($|kr| \approx 1$)

Between the near-field and far-field zones, the behavior E , H and impedance are described by the exact relation in equations (3) and (4). Data in this zone are smoothly transitional for the homogenous-earth case from near to far-field behavior. In non-homogenous environments, the transition zone become complex and dependent upon resistivity contrast. Therefore the CSAMT measurement must be carried out in the far-field zone that the plane-wave analysis technique can be applied.

3.4 Near-field and transition-field correction

The problem in CSAMT method is the distortion of apparent resistivity and phase difference close to the transmitter caused by changing dependence of E and H on the source sounding separation r . In the far field zone, both E and H are proportional to $1/r^3$ (equations 9 and 10) and resistivity is thus independent of r . Close to the source, in near field zone, E decay as $1/r^3$ (equation 6) and H as $1/r^2$ (equation 7), making resistivity a function of geometry. At intermediate distance, in transition zone, E decay as $1/r^3$ (equation 3) and H decay as intermediate rate between $1/r^2$ and $1/r^3$ (equation 4). In this paper, the definition of far field zone is essentially free from nonplane-wave source effect less than 10 percent of the total response in the Cagniard resistivity parameter. The near field zone as the area where E and H are completely saturated and H decay as $1/r^2$. The area between them is the transition zone.

The plane-wave aspects of the CSAMT technique have been examined in detail by previous authors^{1,4)}. They have shown that under proper field (far field) conditions, the apparent resistivities calculated from CSAMT measurements using equation (11) are similar to the plane-wave apparent resistivities. For E measured parallel to the direction of the transmitting bipole, the area of investigation should be at least three skin depths from the transmitter for broadside configuration (the electric field parallel to the transmitter bipole on its center line) as shown in **Fig. 4(a)**. The proper distance increases to five skin depths

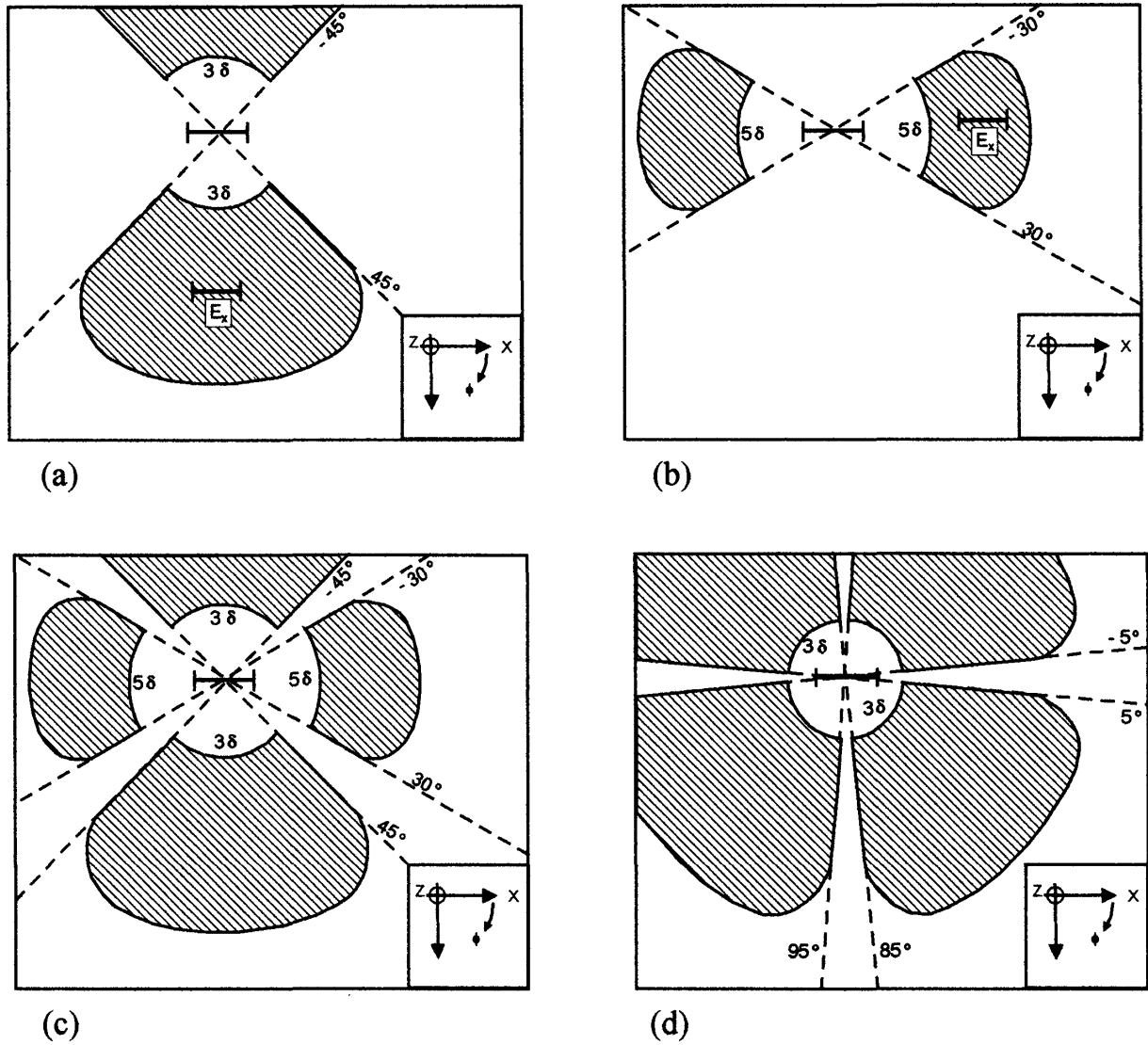


Fig. 4 (a) Broad side configuration, (b) Collinear configuration, (c) Acceptable zones of CSAMT measurement (shaded-area) for E_x / H_y and (d) Acceptable zones of CSAMT measurement (shaded-area) for E_y / H_x ⁶⁾.

for collinear configuration (the electric field parallel to the transmitter bipole on its axis) as shown in **Fig. 4(b)**. Moreover, Zonge and Hughes⁶⁾ described the acceptable zones of data acquisition for CSAMT measurements as presented in **Fig. 4(c)** and **(d)**.

Because of the need to minimize the transmitter-receiver separation for maximum signal, the far-field zone is restricted by this situation, therefore most CSAMT data sets will contain some near-field and transition zone data. To overcome the source effect problem, a correction technique to CSAMT data should be applied to obtain apparent resistivity value equivalent to the far field situation. In this paper, we used a simple technique to correct near-field CSAMT apparent resistivity proposed by Yamashita¹⁸⁾, that is, the plane wave apparent resistivity is apparent resistivity calculated by near field equation for the lower frequency and apparent resistivity calculated by Cagniard equation for the high frequency.

3.5 2-D inversion of MT

2-D inversion has been used to interpret MT data. This technique makes the interpretation more objective and less time-consuming than the trial-and-error approach but it does not yield a unique solution. Despite this, a common approach to fitting a 2-D MT data set is to

construct a cross-section of the area based on prior geological knowledge and the model parameterization to solve for the conductivities by least-square inversion¹⁹⁾. Recently, many useful 2-D MT inversion schemes have been developed. Among the many studies reported, the smoothness-constrained (“regularized” solution) least-squares method for 2-D MT inversion, which finds the smoothest change to the model and the residual error lies within a desired tolerance, was developed by Sasaki²⁰⁾, deGroot-Hedlin and Constable²¹⁾ (Occam’s inversion), Smith and Booker²²⁾ (Rapid relaxation inversion), and Uchida²³⁾ (Smoothing with Akaike’s Bayesian information criterion). All of the methods belong to the group with the most rigorous non-linear approach to calculate the 2-D Frechet derivative.

In this paper, we carried out 2-D inversion of MT data of transverse magnetic mode using the algorithm proposed by Rodi and Mackie¹⁰⁾ that is a non-linear conjugate gradients (NLCG) algorithm. The NLCG scheme is to minimize an objective function containing data residuals and the second spatial derivatives of resistivity.

Tikhonov’s method defines a regularized solution of the inverse problem to the model m that minimize the object function is¹⁰⁾

$$\phi(m) = (d - F(m))^T V^{-1} (d - F(m)) + \lambda \|L(m - m_0)\|^2 \quad (12)$$

where d is observed data vector, m is an unknown model vector, m_0 is a priori model, F is a forward modeling operator, V is an error covariance matrix, L is a linier operator, and λ is a regularization parameter. Each datum d_i is log amplitude or phase of transverse electric (TE) or transverse magnetic (TM) mode of complex apparent resistivity at a particular station and frequency. The model vector is also log resistivity as a function of position ($m(x) = \log \rho(x)$). Laplacian operator can be written as follow

$$\|L(m - m_0)\|^2 = \int (\Delta(m(x) - m_0(x)))^2 dx \quad (13)$$

NLCG directly solves to minimize the objective function ϕ of equation (13). The model sequence is given by

$$\phi(m_j + \alpha_j h_j) = \min_{\alpha} \phi(m_j + \alpha h_j) \quad (14)$$

$$m_{j+1} = m_j + \alpha_j h_j \quad (15)$$

$$h_j = -C_j g_j + \beta_j h_{j-1} \quad (16)$$

where α_j is the step size, h_j is the search direction, C_j is the preconditioner, g_j is the gradient of objective function and β_j is the scalar calculated as

$$\beta_j = \frac{g_j^T C_j (g_j - g_{j-1})}{g_{j-1}^T C_{j-1} g_{j-1}} \quad (17)$$

In NLCG algorithm, the preconditioner has a big impact on efficiency. Two competing considerations in its choice are the computational cost of applying the preconditioner, and its effectiveness in “steering” the gradient vector into productive search direction.

4. CSAMT data interpretation

4.1 Two-dimensional inversion results

According to the results obtained through the 2-D inversion results of CSAMT data in TM mode, the 2-D resistivity section for each profile can be constructed (**Figs. 5-8**). Generally, the Takigami area is composed mainly of three layers of resistivity structure. The surface layer (first layer) has a resistivity of 30–500 ohm-m and the thickness of 200–500

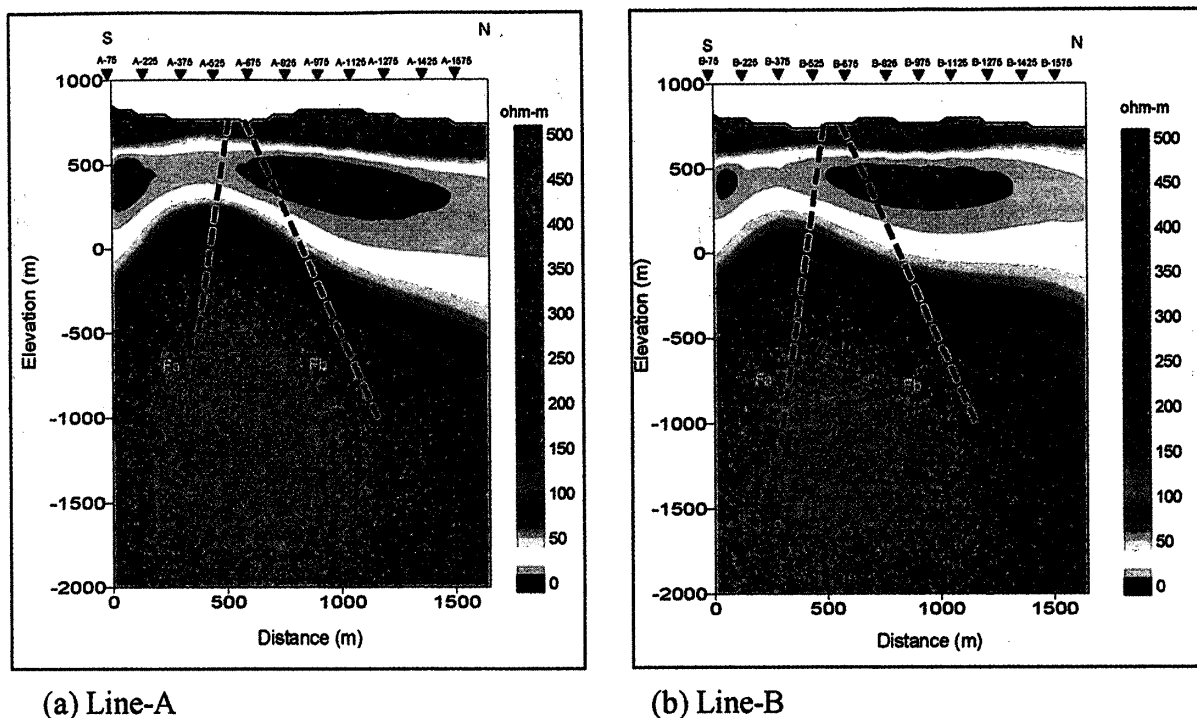


Fig. 5 Resistivity profiles (S-N direction) based on 2-D inversion of CSAMT data with electrical discontinuities Fa and Fb.

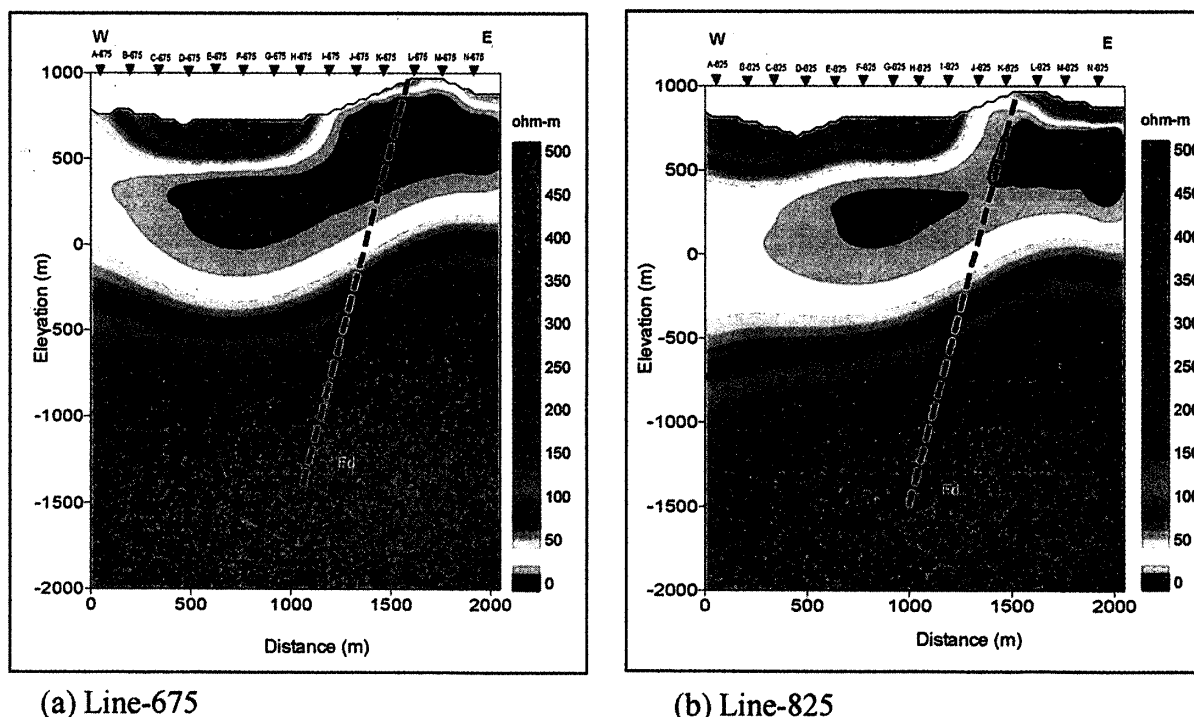


Fig. 6 Resistivity profiles (W-E direction) based on 2-D inversion of CSAMT data with electrical discontinuity Fd.

meters overlying an extremely low resistivity zone (second layer), which has a resistivity value of 3-15 ohm-m and a thickness of 500-800 meters. This second layer correlates with a strong hydrothermal alteration zone. The bottom layer (third layer) has a resistivity value of 30-500 ohm-m that is more resistive than the second layer.

Figure 5 shows the 2-D resistivity sections in south to north direction of Line-A (Fig. 5(a)) and B (Fig. 5(b)) with survey lines as shown in Fig. 2. There are two types of the

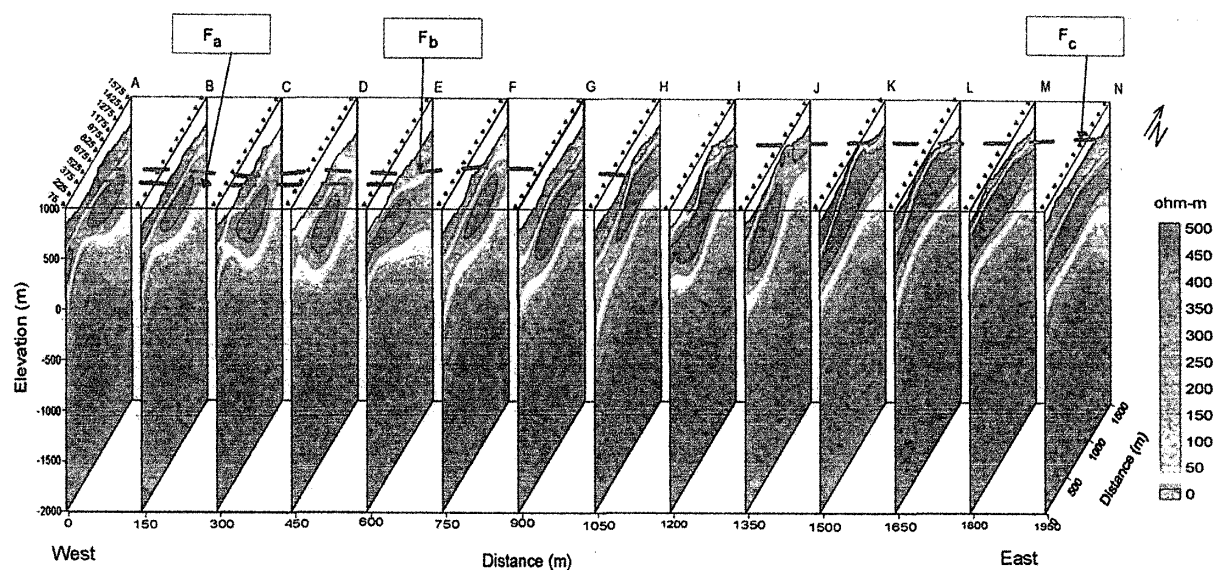


Fig. 7 Resistivity section of 2-D inversion results (W to E direction).

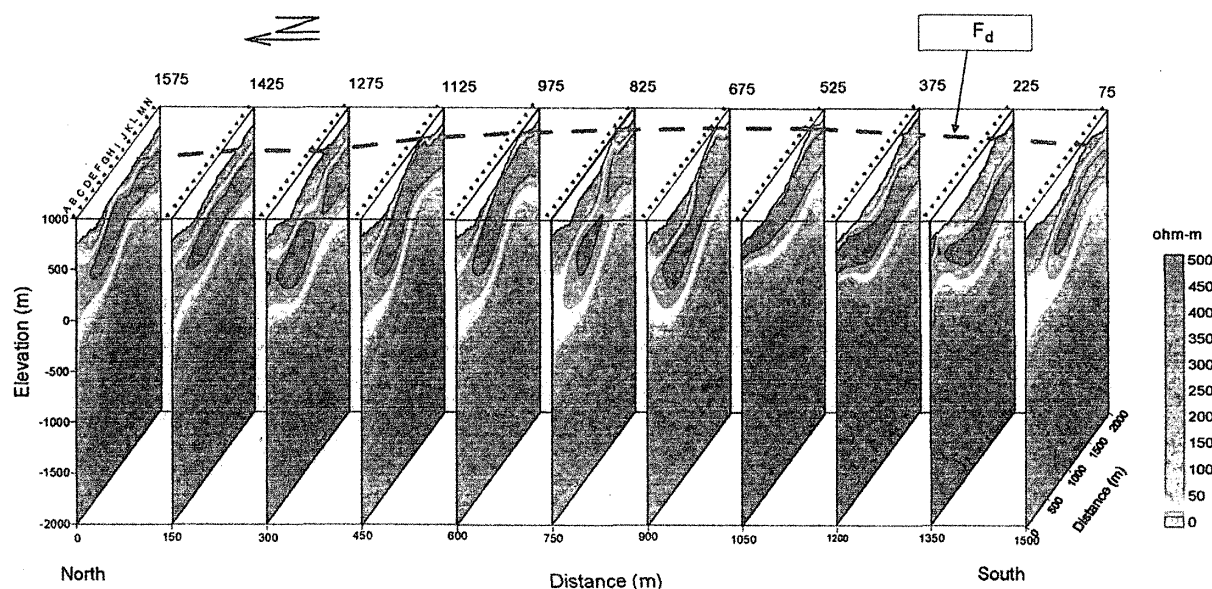


Fig. 8 Resistivity section of 2-D inversion results (N to S direction).

electrical discontinuities found in those lines, that is Fa and Fb. The electrical discontinuity Fa clearly can be seen in the southwestern part of the survey area that is coincident with Teradoko fault. On the other hand, Fb is a remarkable electrical discontinuity in the area where the low resistivity is distributed broadly in the area in which the possible and close relation of a high geothermal activity may exist. The electrical discontinuities Fa and Fb extend from west to east up to Line-E and Line-H, respectively (Fig. 7). In west to east direction, it is recognized also the electrical discontinuity Fc, which is located in the center of survey area from sites I-825 to N-825 (Fig. 7). This area also has a high possibility of presence of geothermal reservoir.

2-D resistivity sections of Line-675 and Line-825 in west to east direction are also displayed in Fig. 6. The figure shows that there is electrical discontinuity Fd which is shown clearly below site K-675 (Fig. 6(a)) and K-875 (Fig. 6(b)). The Fd is also a remarkable electrical discontinuity because it is coincident with the position of Noine fault zone, extending from south to north (Fig. 8). This fault divides the area into two parts, western and

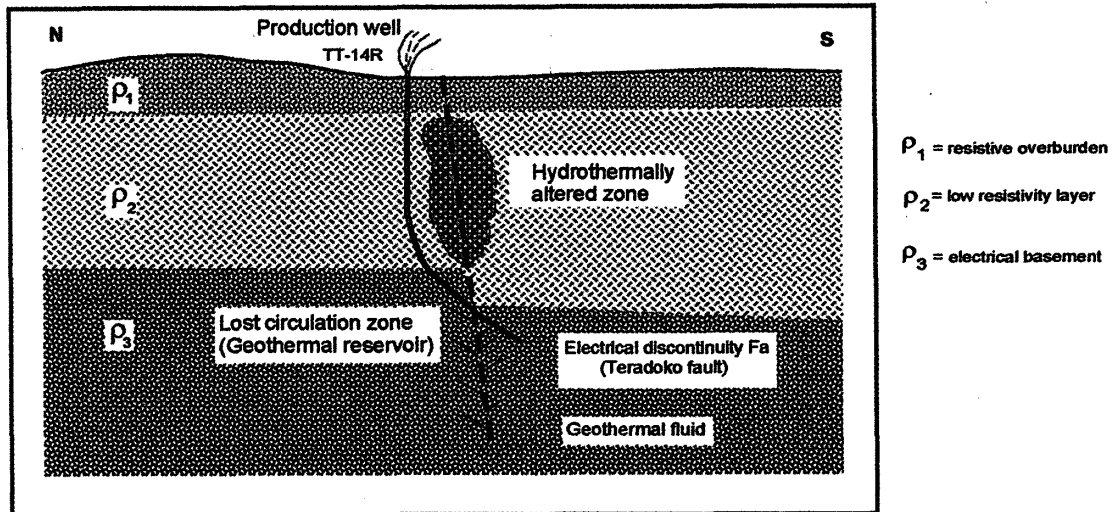


Fig. 9 Geoelectrical model of fractured type geothermal reservoir.

eastern part. It is clearly shown in the Figs. 6(a) and (b) that the distribution of low resistivity is shallow and thin in the east and deepen and become thicker in the west. Accordingly, the underlain resistive layer correlated to the reservoir zone is shallower in the eastern part than that in the western part. This condition is similar with the interpretation of MT results for the survey line of SW-NE direction that the low resistivity in the second layer is shallow and thin in the northeast and become deeper and thicker in the southwest. The boundary of this condition is a Noine fault zone⁷⁾. From these results, it may conclude that the geoelectrical structure of fractured type geothermal reservoir can be explained by the model as shown in the Fig. 9.

The deep circulation of high temperature and pressure geothermal fluid along fracture zones will transfer heat to shallower level, and concentrating it into shallow reservoirs or discharging as hot springs. This process extends to lateral direction and forming the alteration zone.

The electric and electromagnetic exploration methods are more effective to detect a low resistivity zone on the vertical direction correlating with the existing alteration zone. If the low resistivity zone exist in the shallow depth and the electrical discontinuity is found around the low resistivity zone, the geothermal reservoir in the deep can be predicted. Therefore, the geothermal reservoir in Takigami geothermal field may exist around the electrical discontinuities Fa, Fb, Fc and Fd. This condition is similar to a geothermal system in Hatchobaru area obtained from interpretation of resistivity data²⁴⁾.

4.2 Comparison of 2-D inversion results with well log data

To confirm the 2-D CSAMT inversion results, resistivity well log and the temperature data from wells TT-13S, TT-14R, TT-16S and TT-20 are displayed in the Fig.10. The resistivity log data plotted with a semi log scale in ohm-m versus depth is put together in the same scale with the resistivity section. The lost circulation and temperature data are written on the sections.

Figures 10(a) - (d) show the comparison of resistivity sections along wells with the temperature, lost circulation and resistivity log data obtained in the wells. The conductive features (3 - 15 ohm-m) recorded up to 700 m below sea level (BSL) for each section can be attributed to the abundant presence of clay minerals due to hydrothermal alteration. The resistivity of formation increases, and reaches 200 - 300 ohm-m at the depth between 300 and

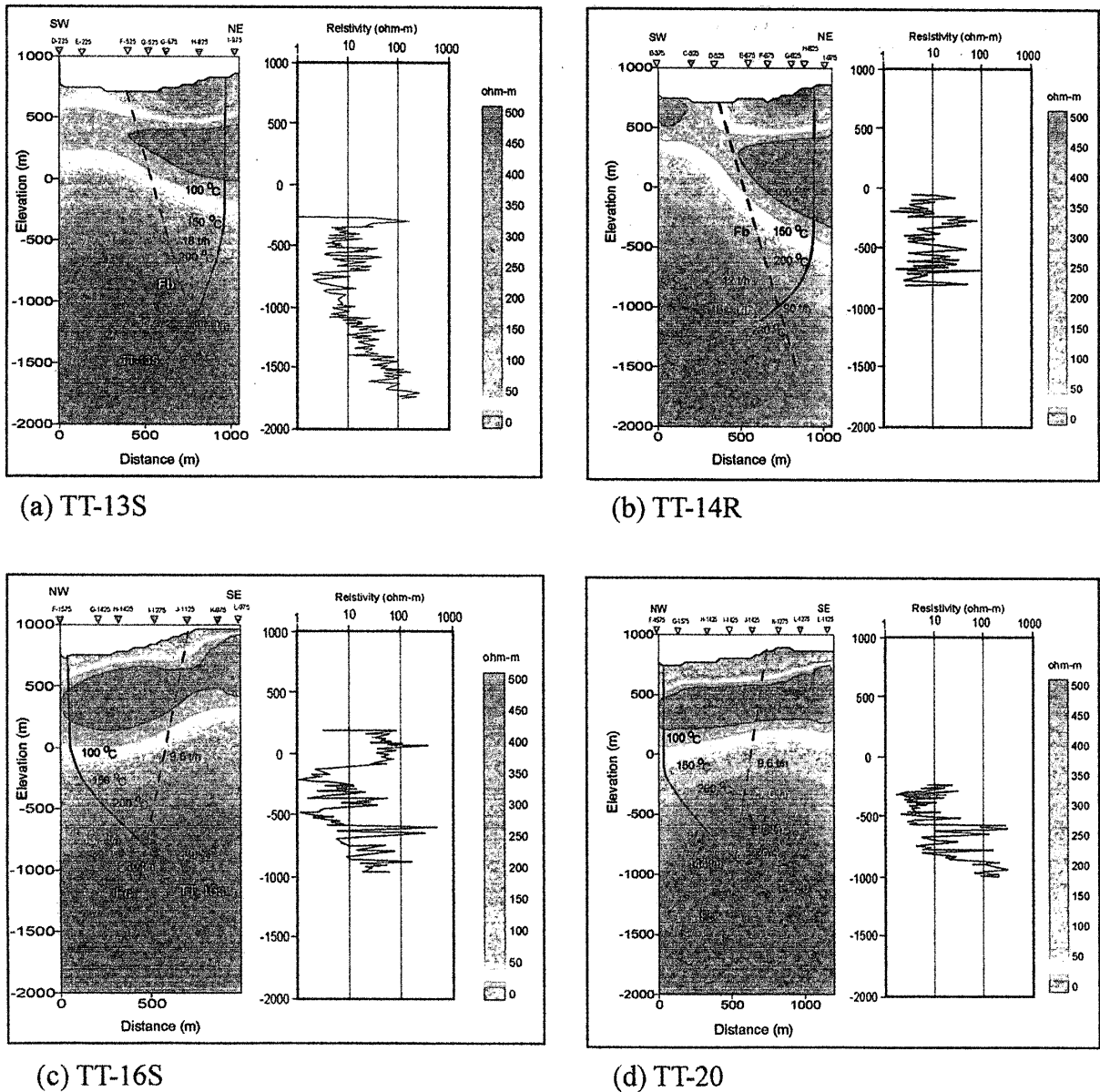


Fig.10 Comparison of 2-D inversion results with the temperature, lost circulation and electrical resistivity log data.

700 m BSL where the reservoir zone may exist in this formation (resistive layer). On the other hand, the resistivity well logs of the wells correspond to 2-D CSAMT inversion.

The subsurface temperature distributions obtained from fluid inclusion measurement using rock samples from the wells (TT13S, TT-14R, TT-16S and TT-20) are displayed on the resistivity sections as shown in the **Figs.10(a) - (d)**. At the conductive zone, the low temperature (100°C) clay mineral such as montmorillonite is dominated. The temperature increases rapidly from 100 to 200°C at depth range of 0 to 400 m BSL that the temperature gradient is steep in this zone. Below 700 m BSL, the temperature distribution for each well becomes high with the temperature range from 230°C (for TT-14R, TT-16S and TT-20) to 250°C (for TT-13S). Therefore, this layer is expected as a reservoir zone. The temperature distributions from each well have a good correlation to the resistivity distribution for each section derived from 2-D inversion.

The lost circulation of 18 ton per hour (t/h) was found in the depth of 500 m BSL for TT-13S (**Fig.10(a)**). For TT-14S, the lost circulation of 12 t/h occurred at the depth of 600

m BSL (**Fig.10(b)**). The lost circulation of 13.8 t/h was found at the depth of 200 m BSL for TT-16S and TT-20 (**Figs.10(a)** and **(b)**). The interesting point is found that the large lost circulation occurred at the depth of 1200 m BSL for the well TT-13S (114 t/h) and at the depth of 1300 m BSL for the well TT-14R (90 t/h) when the well crossed through the electrical discontinuity Fb in well TT-13S and TT-14R below the sounding site G-675 and G-825, respectively. Therefore, the electrical discontinuity Fb can be considered to indicate the presence of fault. On the other hand, the large lost circulation was found at the depth of 1000 m BSL for TT-16S and TT-20 with amount of 210 and 144 t/h mud, respectively, during the course of drilling. These high mud-water loss was encountered when the drilling well crossed through the electrical discontinuity Fc in the well TT-16S (**Fig.10(c)**) and TT-20 (**Fig.10(d)**) under CSAMT sites J-1125 and J-1425, respectively. Thus, the electrical discontinuity Fc also has a high possibility of promising fractures.

5. Conclusions

Employing a 2-D inversion to CSAMT data, we have successfully obtained the reasonable resistivity structure. The results are compared to real geological condition confirmed by drilling and indicated four remarkable electrical discontinuities that may correlate with fractures in the area. Highly correlation has been found between 2-D inversion results and well log data (electrical resistivity log, temperature and lost circulation data). Especially, the electrical discontinuities obtained from 2-D resistivity section are coincided with the zones of good lost circulation, which can be considered to highly indication of potential fractures.

Generally, the subsurface resistivity structures in Takigami geothermal filed are composed mainly by three types of resistivity feature, which are supported by both the 2-D inversion results of CSAMT data and resistivity logs (**Figs.10(a) - (d)**). The features of resistivity structure correlating with type of rocks and temperature distributions can be explained as follows,

- The overburden (first layer) has a resistivity of 30 - 500 ohm-m and thickness of 300 to 500 m. This layer correlates with Noine-dake volcanic rock as non-altered zone and low temperature zone (50°C) due to cold meteoric water circulation.
- The intermediate (second) layer has an extremely low resistivity of 3 - 15 ohm-m that is 800 - 1000 m thick. The low resistivity layer as an anomalous feature can be considered as a hydrothermal alteration zone (impermeable layer/cap rock). The second layer corresponds to Kusu, Ajibaru and Takigami formation composed of smectite and mixed clay minerals. The temperature distribution in the layer is characterized by a steep thermal gradient of about 20°C/100 m.
- The basement (third) layer is relatively more resistive than the second layer with resistivity of 30 - 500 ohm-m. This layer correlates with Mizuwake andesite rock, an illite-chlorite layer and high temperature zone (160 - 250°C).

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